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ALESEP: A Computer Program for the Analysis of Airfoil Leading Edge Separation Bubbles

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ALESEP: A Computer Program for the Analysis of Airfoil Leading Edge Separation Bubbles

SUMMARY

A program called ALESEP is presented for the analysis of the inviscidviscous interaction which occurs due to the presence of a closed laminartransitional separation bubble on an airfoil. The ALESEP code provides an iterative solution of the boundary layer equations expressed in an inverse formulation coupled to a Cauchy integral representation of the inviscid flow. This interaction analysis is treated as a local perturbation to a known solution obtained from a global airfoil analysis; hence, part of the required input to the ALESEP code are the reference displacement thickness and tangential velocity distributions. Special windward differencing may be used in the reversed flow regions of the separation bubble to accurately account for the flow direction in the discretization of the streamwise convection of momentum. The ALESEP code contains both a forced transition model based on a streamwise intermittency function and a natural transition model based on a solution of the integral form of the turbulent kinetic energy equation. Instructions for the input, output, and program usage are given herein along with a sample case.

LIST OF SYMBOLS

a	Structural coefficient
c .	Airfoil chord
c _f	Skin friction coefficient
D	Damping factor applied to mixing and dissipation lengths
f	Perturbation stream function
F	Velocity ratio, u/u _e
g	Total enthalpy ratio, H/H _e
Н	Total enthalpy
l	Mixing length or ratio of local to edge density * molecular viscosity product
L	Reference length or dissipation length
m	Perturbation mass flow
n	Coordinate normal to reference displacement surface
N	Coordinate measured normal to reference displacement surface fro the body surface
Pr	Prandtl number
PrT	Turbulent Prandtl number
\bar{q}	Magnitude of fluctuating velocities
Re	Reference Reynolds number
Re θ	Local momentum thickness Reynolds number
$\mathbf{\tilde{R}}_{\Theta}$	Correlated momentum thickness Reynolds number
R_{τ}	Turbulent Reynolds number
s,S	Coordinates along reference displacement surface
Tu	Turbulence level
u	Velocity component parallel to reference displacement surface
v	Velocity component normal to reference displacement surface

- V Transformed normal velocity in Prandtl transposition theorem
- α Windward differencing weighting operator
- β Pressure gradient parameter
- δ Boundary layer thickness
- δ^* Displacement thickness
- δ_{τ} Stress thickness
- ε Eddy viscosity coefficient
- K von Karman constant
- η Transformed normal coordinate
- V Kinematic viscosity coefficient
- μ Molecular viscosity coefficient
- ξ Transformed tangential coordinate
- Velocity potential
- ρ Density
- ψ Stream function
- ω Interaction relaxation parameter

Subscripts

- e Edge of boundary layer
- I Inviscid
- ref Reference solution
- t₁ Start of transition
- t₂ End of transition
- T Turbulent
- v Viscous
- ∞ Free stream
- 1 Start of interaction region

2 End of interaction region

Superscripts

- Perturbation quantity
- + Inner wall non-dimensionalized coordinate
- k Global inviscid-viscous iteration counter

GENERAL DESCRIPTION

Introduction

It was pointed out by Tani (Ref. 1) that airfoils at moderate incidence angles, prior to either leading edge stall or thin airfoil stall, experience local separation bubbles just downstream of the peak suction (minimum pressure) regions. Figure 1 shows a schematic diagram of an airfoil leading edge bubble which occurs if the Reynolds number is sufficiently low so that the boundary layer remains laminar up to the minimum pressure point. Downstream of this point, separation occurs almost immediately since laminar boundary layers, in contrast with turbulent flows, are extremely sensitive to adverse pressure gradients. A separation bubble forms in which a recirculating streamline pattern is bounded by a shear layer. Since shear layer flows tend to be highly unstable to flow disturbances, transition from laminar to turbulent flow generally occurs in this shear layer. Further downstream, the turbulent mixing between the shear layer flow with the lower dead air region results in entrainment of higher energy air which energizes the flow near the surface thereby resulting in flow reattachment with subsequent turbulent boundary layer flow downstream. As shown in Fig. 1, the initial position of the separation bubble is characterized by a pressure plateau followed by a pressure recovery region after the transition process is initiated, but prior to flow reattachment.

Technical Approach

The approach taken in the ALESEP code for the analysis of closed leading edge separation bubbles is based on an inviscid-viscous interaction technique in which the boundary layer equations are solved iteratively with an inviscid analysis through displacement thickness coupling. Experimental studies (Refs. 2-5) have shown that these closed transitional separation bubbles occupy only a few percent of the airfoil chord. Since the resultant interaction is highly localized, the leading edge transitional bubble problem is treated as a linear perturbation to a known global airfoil solution. The use of a perturbation approach permits an accurate analysis of the flow field structure in this region in contrast with the extremely difficult problem of trying to resolve this small scale phenomena while simultaneously solving the global airfoil flow field. In contrast with previous perturbation treatments of this problem, the approach taken in ALESEP accounts for the influence of the global viscous airfoil flow on the local interaction analysis. A detailed discussion of the approach taken in the ALESEP technique can be found in Refs. 6-8.

The local inviscid analysis in the ALESEP procedure assumes that the disturbance field induced by the presence of a transitional separation bubble can be treated as a small disturbance to the global airfoil flow. An asymptotic analysis is presented in Ref. 8 which formally shows that under a particular limiting condition, the disturbance field induced by the transitional displacement surface can be represented by a distribution of

sources placed along a reference displacement surface as shown in Fig. 2. The reference displacement surface is usually defined as the displacement thickness which would exist in the local region due to an attached turbulent boundary layer. It, as well as the reference velocity distribution, are obtained from an airfoil analysis code such as that presented in Refs. 9 or 10 in which instantaneous transition from laminar to turbulent flow is assumed to occur at the predicted laminar separation point. Calculation of the perturbation velocity which occurs due to the difference between the separation bubble displacement thickness and the reference displacement surface as shown in Fig. 2, is performed through a Cauchy integral of the streamwise distributed sources using potential flow considerations. Upon integration of this Cauchy integral for the perturbed velocity, the local inviscid velocity distribution, uell, due to the interaction with the separation bubble is determined by adding the perturbation velocity and the reference velocity solution.

The viscous solution technique used in ALESEP is the inverse boundary layer procedure presented by Carter (Ref. 11). In this procedure, a perturbation stream function is introduced into the boundary layer equations for the simplification of boundary conditions. The continuity equation is eliminated and the stream function definition is subsequently added to the governing equation set which also included the momentum and energy equations. The governing equations are solved for the local perturbation stream function, velocity ratio, total enthalpy ratio, and viscous edge velocity, \mathbf{u}_{ev} , for a prescribed streamwise distribution of perturbation mass flow, $\mathbf{m} = \rho_{\text{eu}} \delta^*$. The numerical solution of the governing equations is obtained using an implicit finite difference technique which is first order accurate in the streamwise direction and second order accurate in the normal direction.

Since the boundary layer equations are parabolic, an instability will arise when the solution marching direction is opposite to the flow direction. Reyhner and Flugge Lotz (FLARE) (Ref. 12) have shown that this instability is easily avoided by assuming that the streamwise convection terms are zero in reversed flow regions. It is apparent, however, that a loss of accuracy in the converged solution is incurred due to the negligence of the streamwise convection terms. As an improvement to the FLARE approximation, a windward finite difference operator may be used in the ALESEP code to calculate the streamwise gradient terms in reversed flow regions. The effects of using the more accurate windward differencing scheme are described in detail in Ref. 8.

The transition from laminar to turbulent flow in the separated shear layer may be modeled using one of two possible techniques available in the ALESEP code. A simple forced transition model in which the onset and length of transition are specified may be used in conjunction with either the Cebeci-Smith (Ref. 13) or the McDonald-Fish-Kreskovsky (Refs. 14 and 15) turbulence models. The forced transition model is based on the streamwise intermittency distribution which was established by Dhawan and Narasimha (Ref. 16). Alternately, the natural transition model of McDonald and Fish (Ref. 14) may be used with the McDonald-Fish-Kreskovsky turbulence model to automatically predict the transition location. Details of these

transition and turbulence models in conjunction with the ALESEP inviscidviscous interaction technique may be found in Refs. 6-8.

The present interaction iteration procedure is based on the inviscid-viscous iteration technique presented by Carter (Ref. 17) and is adopted to the present scheme as outlined in Fig. 3. The key feature of this iteration procedure is that the update formula permits the inverse boundary layer analysis to be directly linked to the inviscid analysis which accounts for displacement thickness effects. It was found by Kwon and Pletcher (Ref. 18) that convergence could be accelerated by making several inner loop passes through the Cauchy integral and the update formula with the boundary layer prediction of the edge velocity frozen at its current global iteration value. This technique is used in the present interaction iteration and has been found to significantly accelerate the global convergence rate of the scheme.

USER INSTRUCTIONS

Code Description

A flow chart of the ALESEP code is shown in Fig. 4. The code has been written to allow for one of two possible modes of operation to be performed. The first mode allows for a direct finite difference boundary layer calcuation for a prescribed edge velocity distribution. The second mode allows for an inviscid-viscous interaction calculation for a prescribed reference displacement surface and reference edge velocity distribution.

The ALESEP code is written in FORTRAN IV language and takes 206,000 octal word storage locations. Typically 20-40 global inviscid-viscous iterations are required to reduce residuals in inviscid-viscous edge velocities to 10^{-3} . On a Cyber 175 computer using the Cebeci-Smith turbulence model, an inviscid-viscous interaction calculation takes approximately 12 seconds per iteration. Using the McDonald-Fish-Kreskovsky turbulence model, an interaction calculation takes approximately 80 seconds per iteration. This increase in computing time is a result of the iterative solution of the turbulent kinetic energy equation required for this model.

Input Description

The input to the ALESEP code is read in five separate blocks. The first block is a namelist file, MASTER, used to define parameters which control the mode of operation, the streamwise computational grid, and input/output options. The second block of input contains the prescribed reference pressure, reference displacement surface, and free stream turbulence level distributions. The third input block is a namelist file, INPUT, which defines the controlling parameters for the boundary layer solution procedure. The fourth block is used to define experimental data which may be used in subsequent plots of the results. Finally, the last block of information required for inviscid-viscous interaction cases is the velocity ratio, perturbation stream function, total enthalpy ratio, and eddy viscosity profiles at the inital station of the interaction region and the initial guess of the perturbation mass flow distribution.

The first three blocks of input information are necessary to execute a direct boundary layer calculation. The input variable, IFIN, located in the MASTER namelist must be set to 2 and INVRSE in the INPUT namelist must be set to 0. The computational grid is determined by the following variables:

Streamwise - IGRID, AK1, AK2, DS, MMAX, SSWTCH, SPIVOT, IPIVOT, AK11, AK12, IVGINX, IMAX (namelist MASTER)

Normal - DETA, AK, NMAX1 (namelist Input)

A laminar similarity solution is used at the initial station with a freestream Mach number, AMES, and gradient, BETAS = $(1/M_e)(dM_e/d\xi)$ prescribed in namelist INPUT. The user has a choice of transition and turbulence models through the definition of variables, STRANS, KTRAN, TRNLEN, and ITRBMD located in namelist INPUT. For ITRBMD = 0, the Cebeci-Smith turbulence model is used with forced transition occurring according to specified values of STRANS, KTRAN, and TRNLEN. For ITRBMD = 1 or 2, the McDonald-Fish or McDonald-Fish-Kreskovsky natural transition turbulence model is used and transition is predicted automatically.

For an inviscid-viscous interaction calculation, input blocks 1, 2, 3 and 5 are necessary. The input variable, IFIN, located in namelist MASTER, must be set to 3 and INVRSE in the INPUT namelist must be set to 1. A total of IQUIT global inviscid-viscous iterations are performed. The structure of the computational grid is determined by the same variables previously mentioned for a direct boundary layer calculation with some required constraints which are discussed below. Velocity ratio, perturbation stream funtion, total enthalpy ratio and viscosity profiles at the initial station of the interaction region are required in the fifth input block (NSTART=1 in INPUT namelist) and are obtained from a direct boundary layer calculation extending from the leading edge to the initial station of the inviscid-viscous interaction calculation located somewhat ahead of the laminar separation point. For INTERP=0 in namelist INPUT, the values of AK and NMAX1 which define the computational grid in the normal direction in namelist INPUT should be the same as that used in the direct boundary layer calculation. The value of DETA in namelist INPUT should be the value used in the direct boundary layer calculation scaled by $\sqrt{2\xi/\rho_e} u_e r_o^i \delta^*$ due to the different definitions of the normal coordinate used in the direct and inverse boundary layer formulations. This scaling is performed automatically in subroutine CONVRT at the last computational station of the direct boundary layer calculation when IPRNEW has been set to 1. The value of DETA for the interaction calculation can then be found in the converted profile information for the last station printed out at the end of the direct boundary layer calculation. The value of XCO in namelist INPUT for the interacting calculation should be defined as the value of XC at the last computational station of the direct calculation. The value of AHO also in namelist INPUT should be defined as the value of AH at the last computational station of the direct calculation scaled by the inverse over direct DETA ratio. As in the direct calculation, the user has a choice of transition and turbulence models through definition of the input variables STRANS, KTRAN, TRNLEN, and ITRBMD. In addition to the models described in the direct boundary layer calculation, a forced transition model may be used with the McDonald-Fish (Ref. 14) or McDonald-Fish-Kreskovsky (Ref. 15) turbulence models by setting KTRAN=IQUIT and defining STRANS and TRNLEN. To use the natural transition model of McDonald and Fish with these turbulence models, KTRAN must be set to 0. Special windward differencing may be used in the reverse flow region of the separation bubble through definition of IWINDD and IWINDG in namelist INPUT. Detailed results using the different turbulence models and windward differencing scheme may be found in Refs. 6-8.

Detailed Input Description

Input Block 1:

The first block of input is read in from subroutine Main in a namelist called MASTER. This information defines the streamwise computational mesh and parameters controlling input and output.

INPLT	Number of global iterations between calls to plotting routines.
IQUIT	Total number of global inviscid-viscous iterations to be computed. Set IQUIT=1 for a direct boundary layer calculation.
RFDT	Relaxation factor applied to the perturbation mass flow in the inviscid-viscous update procedure.
RFVN	Relaxation factor for the injection velocity to represent viscous effects (inactive, set = 1.0).
MMAX	Total number of streamwise grid points used in the boundary layer calculation.
SSWTCH	Arclength location measured from the nose of the body where the boundary layer calculation is initiated.
IPLOT	Value of the global iteration counter at which the plot subroutines are first called.
AK1	The ratio of adjacent grid sizes used in generating the boundary layer grid in the streamwise direction beginning at SSWTCH.
AK2	The ratio of adjacent grid sizes at SSTING where SSTING > SSWTCH.
SSTING	Location where secondary boundary layer stretching, AK2, in the streamwise direction is initiated.
DS	Increment in arclength used at start of boundary layer mesh which begins at SSWTCH.
IVT1	Index in the inviscid streamwise arrays where the tangential velocity VT is read into program (inactive, set = 0).
IVT2	Last index where VT (I) is read into program (inactive, set = 0).
ISMOTH	If equals zero, no smoothing is used; if equals 1, the smoothed VT distribution is used.

MIT2 Inactive, set = 0.

SSTOP Arclength location measured along the reference surface where the calculation is terminated downstream.

ITEK Inactive, set = 0.

IAXI If equals 0, two dimensional flow; if equals 1, axisymmetric flow.

IFIN If equals 1, program terminates after initial inviscid calculation (this initial inviscid calculation is made with no boundary layer effect). If equals 2, program terminates after initial inviscid calculation and one pass thorugh boundary layer solver. If equals 3, program operates in full interactive mode and terminates after IQUIT iterations.

IFILET If equals 1, the offset distance between the circular arc, hard surface and a cubic filet coordinate surface will be computed (set = 0).

XT1 XT2 XSTING

YSTING Inactive, set = 0.

RADIUS THICK XLO

IWRPMF If equals 0, bypass. If equals 1, the perturbation mass flow distribution is written to unit 13 for later restart.

CHORD Reference length which allows rescaling the original axial distance measured from the nose to an alternate coordinate system measured from another location located at distance XOR from the nose.

XOR Axial location in the original coordinate where the origin of the new coordinate X/C is located. Both XOR and CHORD are used to shift and rescale the axial coordinate used in the program.

Shift factor which allows the inviscid calculation to start at a downstream location on an open nose body where the flow is not disturbed near the nose. SIO is the distance from the original nose of the body to the downstream location where the inviscid calculation is started (set = 0).

IPLTX If equals zero, bypass. If equals 1, then the program generates a plot file which will later generate the plots on a TEKTRONICS unit for studying the resuts of individual iterations. The user may select the global iteration(s) for which plots are to be generated.

NDCP If equals 0, bypass. If equals 1, then experimental CP data versus X will be read into the program and plotted on CALCOMP plot from subroutine PLOTCP.

NDDT If equals 0, bypass. If equals 1, then experimental displacement thickness distribution versus X/C will be read into the program and plotted along with the computed displacement thickness distribution.

NDCF If equals 0, bypass. If equals 1, then experimental skin friction data versus X/C will be read into the program and plotted along with the computed skin friction distribution.

NDUE If equals 0, bypass. If equals 1, experimental tangential velocity data versus X/C will be read in and plotted along with the tangential velocity computed solution.

IPRINT(I) Array containing global iteration values at which station output is printed (array length = 100).

IGRID If equals 0, inviscid and boundary layer mesh are generated by their own parameters.

If equals 1, inviscid mesh is set by its own parameters (IMAX, SINO, AKI1, AKI2, SPIVOT, IPIVOT, IVGINX - as described below) and boundary layer mesh is set equal to the inviscid mesh for S > SSWTCH.

If equals -1, inviscid mesh is set equal to the mesh at which geometry is input (i.e., XO, YO, SO) and boundary layer mesh is set equal to inviscid mesh for S > SSWTCH.

If equals -2, inviscid mesh is set equal to the mesh at which geometry is input and boundary layer mesh is generated by its own parameters.

IMAX Maximum number of points in streamwise direction for the inviscid mesh.

SINO The arclength at first point in inviscid mesh, or SI(1).

AKI1 Ratio of adjacent grid sizes used in generating the inviscid grid in the streamwise direction between SINO and SPIVOT.

AKI2 Ratio of adjacent grid sizes used in generating the inviscid grid in the streamwise direction for S > SPIVOT.

SPIVOT Arclength at which geometric progression constant changes from AKI1 to AKI2.

IPIVOT Streamwise mesh index at SPIVOT.

IVGINX If equals 0, uniform inviscid mesh; if equals 1, a variable mesh using AKI1, AKI2 is used.

LOADDT If equals 0, reference displacement thickness, DTO = 0; if equals 1, DTO is read in the second input block.

LOADSI If equals 0, compute arclength from X0, Y0; if equals 1, arclength is read in the second input block.

LOADCP If equals 0, compute CPO using Cauchy integral; if equals 1, CPO is read in the second input block.

Input Block 2:

The second block of input is read in from subroutine INVO in a formated block. This block of information contains the reference displacement surface, reference velocity distribution, and edge turbulence level distribution.

ITITLE Card 1: A brief title for the configuration (12A6).

IXY Card 2: Number of points at which inviscid input including reference solution is read in. (I3)

XO Card 3: Cartesian distance in horizontal direction.

YO Cartesian distance in vertical direction.

SO Arclength measured from stagnation point.

CPO Pressure coefficient, $(P_0 - P_{\infty})/\frac{1}{2}\rho_{\infty}U^{\frac{2}{\infty}}$, from reference solution.

DTO Displacement thickness from reference solution.

TUO Freestream turbulence level.

NOTE: IXY values of XO, YO, SO, CPO, DTO, TUO are read in (4F10.7, E10.5, F10.7) format.

GAM Card 4: Y, the specific heat ratio.

AMINF M_{∞} , freestream Mach number.

NOTE: GAM, AMINF are read in with 2F10.7 format.

Input Block 3:

The third block of input is read in from subroutine TURBID in a namelist called INPUT. The information in this block is used to define the computational grid in the normal direction, the reference freestream flow conditions, the transition and turbulence model, and further output parameters.

- NMAX1 Total number of grid points which are used across the boundary layer in the normal direction.
- NMXOLD Total number of grid points in the initial profile of the interaction calculation.
- DETA Increment in the transformed normal grid spacing, Δn , adjacent to the wall.
- AK Ratio of adjacent step sizes in the eta, η , direction which is used to generate the mesh across the boundary layer. A uniform mesh (AK=1) is not currently allowed.
- INVRSE If equals 0, then a direct boundary layer calculation is to be performed; if equals 1, then an interacting boundary layer calculation is to be performed.
- JPFMAX Total number of points used in the initial guess for the perturbation mass flow distribution, PMFIN to be read in the fifth input block. In the case of restart, i.e., if IRESTR equal to 1, then JPFMAX should be set equal to MMAX.
- IRESTR If equals 0, bypass; if equals 1, then a restart capability is used. In this case, the input array for PMFIN obtained from a previous calculation are read from unit 12.
- INTERP If equals 0, bypass; if equals 1, then profiles at the initial interaction station are to be interpolated onto the interaction grid (set = 0).
- If equals 0, bypass. If equals 1, the computed profiles at M=MMAX from a direct boundary layer calculation are converted from direct variables to inverse variables. Principally, this involves a change in the stream function and in the transformed normal coordinate eta, η .
- NSTART If equals 0, program is initiated with the solution of the self-similar equations. If equals 1, profiles for the velocity ratio, stream function, total enthalpy ratio, and viscosity versus eta, η , are read from the fifth input block.
- NQMAX Maximum number of column iterations which can be used in the boundary layer solution procedure.

NPRRES If equals 0, bypass; if equals 1, boundary layer residual information will be printed.

MFIG(I) Array of index values of the streamwise stations where profiles in the boundary layer solution are printed (array length = 100).

JMAX The maximum number of boundary layer profiles to be printed out. If JMAX equals zero, then there will be no profiles printed, in which case, MFIG is set to a hundred zeros.

ITPRO Global iteration counter at which detailed boundary layer residual and profile information is printed out.

PMFO Multiplicative factor which is used to rescale the perturbation mass flow.

AHO Initial value of the static temperature integral across the boundary layer which appears explicitly in the boundary layer equations. This parameter is needed when NSTART = 1, i.e., the boundary layer solution is initiated with specified profiles instead of internally generated self-similar solutions.

XCO Initial value of the transformed (Levy Lees) ξ variable which is needed when NSTART = 1.

RESG Maximum change in the dependent variable allowed between successive column iterations $\underline{\mathbf{i}}_{4}$ the boundary layer calculation. Typical value used is 10^{-} .

IPLOT(I) Array containing an index to determine which plots are desired
by the user (array length = 8). If IPLOT(I) is equal to 0, plot
is bypassed; if IPLOT(I) is equal to 1, then the plot is made.
The following order is used in the plotting subroutine. Plot #1
is DT (δ*, displacement thickness) versus X/C. Plot #2 is CF
versus X/C. Plot #3 is UE (VT, the inviscid tangential
velocity) versus X/C. Plot #4 is Beta (pressure gradient
parameter) versus X/C. Plot #5 is VN versus X/C. Plots #6, 7
and 8 control the plotting of profiles across the boundary
layer.

WAKCON The Clauser constant in the Cebeci-Smith eddy viscosity law is SWK1 varied linearly from 0.0168 at S=SWK1 to 0.0168/WAKCON at S=SWK2 (set WAKCON=1.0, SWK1=10000, SWK2=20000 to deactivate this option).

YORIGN(I) Array containing the origin of the Y axis for each of the respective plots listed above (array length = 8).

YSCALE(I) Array containing the scale factor for each of these plots (array length = 8). If the scale factor exceeds 1000, then the scale for these particular plots is determined automatically.

YIN(I) Array containing the number of inches for Y axis in each of the plots listed above (array length = 8).

XIN(I) Array containing the number of inches used along the X axis in the respective plots (array length = 8).

XL Reference dimensional length used to convert the present X to a dimensional distance.

NDATA If equals 0, bypass; if equals 1, experimental data will be read from the fourth input block to be plotted with numerical results.

BETAS Value of the pressure gradient parameter, (1/M)(dM/dS), which is required in the self-similar solution.

AMES Value of the streamwise Mach number required in the self-similar solution.

GW Value of the total enthalpy ratio at the wall.

TINFD Reference temperature at infinity in degrees Rankine which is required in the Sutherland law for molecular viscosity.

PRT Turbulent Prandtl number.

PR Prandtl number.

REINF Reynolds number based on the reference (free stream) properties and based on the length which is used to nondimensionalize the coordinate used in the calculation.

STRANS Nondimensional distance along the body at which instantaneous transition is assumed to occur.

KTRAN For Cebeci-Smith turbulence model - (ITRBMD=0): equal to 0, fully laminar calculation; equal to 1, instantaneous transition occurs at STRANS; equal to 2, transition occurs over TRNLEN starting at STRANS. For McDonald-Fish turbulence model - (ITRBMD=1,2): KTRAN is the global iteration number when the McDonald-Fish natural transition model begins to predict the transition location. Forced transition over TRNLEN starting at STRANS is used for all global iterations prior to KTRAN.

IWINDD Global iteration number when convection windward difference operation is effective.

IWINDG If equals 0, do not use windward differencing in energy equation; if equals 1, use windward differencing on convection terms in energy equation starting on the IWINDD global iteration.

IWINDS If equals 0, do not use windward differencing on stream function; if equals 1, use windward differencing on stream function in momentum and energy equations starting on the IWINDD global iteration. This option is not recommended at this time (set = 0).

ITRBMD If equals 0, Cebeci-Smith turbulence model; if equals 1, McDonald-Fish turbulence model; equals 2, McDonald-Fish-Kreskov-sky turbulence model.

Input Block 4:

The fourth block of input is read in from subroutine TURBID in a formated block only when NDATA $\neq 0$. This block of information contains experimental data which may be plotted along with the numerical results.

IDST									
ICFST	Card 1:	Number of	experimental	data	points	to be	read	for DTE,	
IUST		CFE, or U	l (I3).						

J Card 2: Index of experimental data point (I3).

XDTE

XCF Cartesian distance in horizontal direction for XU1 experimental values of DTE, CFE or U1.

DTE Experimental values of δ^* (NDDT \neq 0)

CFE Experimental values of C_f (NDCF \neq 0)

U1 Experimental values of U_g (NDUE \neq 0)

NOTE: IDST, ICFST, or IUST values of J, XDTE, XCF or XU1 and DTE, CFE, or U1 are read in (13, 2F8.4) format

Input Block 5:

The fifth block of input is read in from subroutine TURBID in a formated

block only when NSTART=1. This block of information contains profiles for the velocity ratio, perturbation stream function, and total enthalpy ratio to be used at the initial station of the interaction calculation. For ITRBMD $\neq 0$, the scalar quantities necessary to initialize the turbulent kinetic energy equation as well as the eddy viscosity profiles are also read in this block. The initial guess distribution for the perturbation mass flow parameter is also read in this formated block.

Values of PSI11, PSI12, PSI31, PSI32, EMFK, ALINF, A1MFK, DTINC, DELTU, and A2MA3 are read in 5F16.8 format when ITRBMD # 0. These variables define the scalar quantities required for the McDonald-Fish-Kreskovsky turbulence model at the inital station of the interaction case. These values are stored in unit 14 of a direct boundary layer calculation when IPRNEW = 1. See the output description section for the definition of these variables.

NMAX values of YNI, EPSBB, and EPSHB in a 3E16.8 format are read next when ITRBMD $\neq 0$. These arrays define the viscosity profiles for the McDonald-Fish-Kreskovsky turbulence model at the initial station. These values are stored in unit 14 of a direct boundary layer calculation when IPRNEW = 1. See the output description for the definition of these variables.

NMXOLD values of NN, ETABD, FBD, PSI, and GBD are read in a 15, 4E16.8 format. These arrays define the velocity ratio, perturbation stream function, and total enthalpy ratio profiles at the initial station. These values are stored in unit 14 of a direct boundary layer calculation when IPRNEW = 1. See the output description section for the definition of these variables.

JPFMAX values of PMFIN in a 7F10.7 format followed by JPFMAX values of SPMF in the same format are read in to define the initial distribution of the perturbation mass flow.

Output Description

An example test case for the NACA 66_3 -018 airfoil tested experimentally by Gault (Ref. 2) at a chord Reynolds number of 2×10^6 and a 0.0 degree angle of attack is given in Appendix A. A comparison between the predicted and experimental pressure distributions is shown in Fig. 5(a). The predicted displacement thickness and skin friction distributions are shown in Figs. 5(b) and 5(c), respectively. In this case, the reference pressure distribution was taken to be the experimental high Reynolds number (Re = 10) case in which transition naturally occurred before laminar separation could take place. A direct boundary layer calculation was run

from the leading edge stagnation point of the airfoil to an s/c = 0.5 using the reference pressure distribution as the edge boundary condition. The velocity ratio, perturbation stream function, total enthalpy ratio, and eddy viscosity profiles were taken at the s/c = 0.5 station from the direct calculation and used as initial profiles for the interacting calculation. The reference displacement thickness was held constant at that value predicted by the direct boundary layer calculation at s/c = 0.5. A total of 99 grid points were distributed evenly between s/c = 0.5 and s/c = 0.99in the interaction calculation. The McDonald-Fish turbulence model was used in this case with transition being forced to occur between s/c = .693and .703. The local edge turbulence level was calculated from a 0.2 percent freestream turbulence level and the local to upstream inviscid velocity ratio using the assumption of frozen turbulence. The FLARE approximation of the streamwise convection was used in this case. Windward differencing was found to have little affect on the predicted results. Further comparisons of predicted results using the ALESEP technique with experimental data may be found in Refs. 6-8.

The notation used in the output of the ALESEP code conforms to that used in the description of the governing equations in Refs. 6-8. A dictionary of the variables used in the output can be found in the following section.

Input Cartesian coordinates of body shape.

Reference Distribution Output

XO. YO.

PMF PMFB

S

XB, YB	
so	Input arclength.
СРО	Input reference pressure coefficient.
DTO	Input reference displacement thickness.
TUO, TUB	Input boundary layer edge turbulence level.
VT	Input boundary layer edge velocity at same location as input body coordinates.
SI	Body arclength measured from stagnation point at nose of body same location as input body coordinates.
XOC	Shifted and rescaled value of axial coordinate, XO. XOC = (XO - XOR)/CHORD

Body arclength measured from stagnation point to boundary layer computational stations.

Input perturbation mass flow paramter, $m = \rho_a u_a r_a^i \delta^*$

(interacting case only).

to

SPMF Body arclength measured from stagnation point to boundary layer stations where perturbation mass flow is defined.

XOCBL Same as XOC, but measured from stagnation point to boundary layer computational stations.

RO If flow is axisymmetric, RO is the body radius; for 2-D flow RO=1.

VTBL Boundary layer edge velocity at boundary layer computational stations.

Similarity Solution Output

NQ Boundary layer column iteration counter.

RES1 Maximum change in dependent variable between two successive column iterations.

AHO Static temperature integral, h.

FNW Normalized wall shear, $\frac{\partial F}{\partial \eta}\Big|_{\eta=0}$ where $F = u/u_e$

ETA Transformed coordinate normal to surface, n.

F Streamwise velocity ratio, $u/u_a = F$.

SF Transformed stream function, \tilde{f} .

G Total enthalpy ratio, $H/H_e = G$.

Initial Profiles

If NSTART equals 0, then the initial profile is the same as the laminar self-similar solution. If NSTART equals 1, then the initial profiles are the same as those which are read in (ETABD = ETA, FBD = F, PSI = SF, GBD = G). Note however that if INTERP equals 1, then these profiles have been interpolated onto a new η -mesh.

Station Output (Summary Chart No. 1)

M Streamwise station index

PMF In direct calculation, this is $\sqrt{2\xi}$ where ξ is the streamwise Levy Lees variable; in an interacting case, this is the prescribed distribution of perturbation mass flow, $m = \rho_0 u_0 r_0^2 \delta^*$.

PMFCHK This is $\rho_e u_e r_0^i \delta^*$; in an inverse calculation, this quantity is a check to see that the computed velocity profiles give the same displacement thickness as that prescribed and thus, in the interacting mode, we should always get PMFCHK = PMF.

BETA Pressure gradient parameter, $\beta = (1/M_e)(dM_e/d\xi)$.

BETCHK Calculated pressure gradient parameter (interacting case only).

UEP Boundary layer edge velocity. In direct mode, UEP is the same as the prescribed VTBL; in the inverse mode, it is computed as part of the solution.

AMACH Boundary layer edge Mach number.

AH Static temperature integral, $h = \int_{0}^{\infty} (T/T_e - 1) d\eta$.

CF Skin friction coefficient based on free stream dynamic head, $C_f = \tau_{U}^*/\frac{1}{2}\rho_{\infty}^*U^{*2}$ where asterisk denotes dimensional quantity.

NMCH Index where inner and outer edge viscosity laws are matched (Cebeci-Smith turbulence model).

RTHETA Reynolds number based on momentum thickness.

McDonald-Fish-Kreskovsky Turbulence Model Output (ITRBMD # 0)

MREF Reference free stream Mach number. Same as AMINF in third input block.

TREFD Reference free stream static temperature. Same as TINFD in INPUT namelist.

TREF Nondimensional reference free stream static temperature.

REYREF Reference free stream Reynolds number. Same as REINF in INPUT namelist.

ME2 Boundary layer edge Mach number at current streamwise station.

UE2 Nondimensional boundary layer edge velocity at current streamwise station.

TE2 Nondimensional boundary layer edge temperature at current streamwise station.

RHOE2	Nondimensional boundary layer edge density at current streamwise station.
TU2	Boundary layer edge turbulence level at current streamwise station.
RO2	Geometry coefficient, RO, at current streamwise station.
QE2	Boundary layer edge perturbation velocity magnitude at current streamwise station.
MUE2	Nondimensional boundary layer edge molecular viscosity at current streamwise station.
ME1	Boundary layer edge Mach number at previous streamwise station.
UE1	Nondimensional boundary layer edge velocity at previous stream-wise station.
TE1	Nondimensional boundary layer edge temperature at previous streamwise station.
RHOE1	Nondimensional boundary layer edge density at previous stream-wise station.
RO1	Geometry coefficient, RO, at previous streamwise station.
QE1	Boundary layer edge perturbation velocity magnitude at previous streamwise station.
ACLINF	Free stream dissipation length, L, at current streamwise station.
ALINFN	Free stream mixing length, ℓ , at current streamwise station.
ALINFO	Free stream mixing length, ℓ , at previous streamwise station.
A1MFKN	Structural coefficient, a ₁ , at current streamwise station.
A1MFKO	Structural coefficient, a ₁ , at previous streamwise station.
A2MFK	Structural coefficient, a2, at current streamwise station.
A3MFK	Structural coefficient, a3, at current streamwise station.
BLTHK	Boundary layer thickness at current streamwise station scaled by $\sqrt{R_{\mbox{\scriptsize e}_{\infty}}}$.
DELIN	Inner boundary layer thickness at current streamwise station.
DELTU2	Value of turbulent displacement thickness, $\boldsymbol{\delta}_{\tau}$, at current streamwise station.

DELTU1 Value of turbulent displacement thickness, δ_{τ} , at previous streamwise station.

DTINC2 Incompressible displacement thickness at current streamwise station.

VEDGE Nondimensional boundary layer edge normal velocity component, $v_{\rm e},$ at current streamwise station.

NDELTU Index of normal grid point where DELTU2 is located.

NINNER Index of normal grid point where DELIN is located.

PSIIIN Value of first set of terms of the ϕ_1 integral in turbulent kinetic energy equation at current streamwise station.

PSI12N Value of second set of terms of the ϕ_1 integral in the turbulent kinetic energy equation of the current streamwise station.

PSII10 Value of first set of terms of the ϕ_1 integral in the turbulent kinetic energy equation at the previous streamwise station.

PSI120 Value of second set of terms of the ϕ_1 integral in the turbulent kinetic energy equation at the previous streamwise station.

PSI21N Value of the ϕ_2 integral in the turbulent kinetic energy equation at the current streamwise station.

PSI31N Value of the first set of terms of the ϕ_3 integral in the turbulent kinetic energy equation at the current streamwise station.

PSI32N Value of the second set of terms of the ϕ_3 integral in the turbulent kinetic energy equation at the current streamwise station.

EMFK Value of the source term, E, in the turbulent kinetic energy equation at the current streamwise station.

RTAU Value of the turbulent Reynolds number, R_{τ} , at the current streamwise station.

RTHEAT Value of the correlated momentum thickness Reynolds number, R_{θ} , at the current streamwise station.

A2MA3N Value of the difference of structural coefficient, a2-a3, at the current streamwise station.

Profile Output

ETA Transformed normal coordinate, η.

YBL Nondimensional physical distance from surface.

F2 Streamwise velocity ratio, u/u_p.

SF2 Transformed stream function, f.

G2 Total enthalpy ratio, H/H₂.

EPSBAR $1 + \epsilon/\mu$ where ϵ is the eddy viscosity coefficient and μ is the

molecular viscosity coefficient.

RHOMUR $\ell = \rho \mu / \rho_e \mu_e$.

T Static temperature ratio, T/T_e .

For ITRBMD # 0, the following additional profiles are printed:

YN Nondimensional physical distance from the surface scaled by $\sqrt{\mathrm{Re}_{\infty}}$

YPLUS Nondimensional scaled distance from the surface, y+ =y $\sqrt{\tau/\rho/\nu}$

DUDY Nondimensional velocity normal gradient, 3F/3YN

TAU Shear stress, $(\mu + \mu_{\mathbf{T}}) \partial u / \partial YN$

DAMP Damping factor squared, \mathcal{D}^2 .

FUN Local mixing length distribution in normal direction.

FMFK McDonald-Kreskovsky function, f, on mixing length formula.

Station Output (Summary Chart No. 2)

M Streamwise index.

XLE Cartesian coordinate of station location.

DT* Scaled displacement thickness, δ * \sqrt{Re} .

THETA* Scaled momentum thickness, $\theta \sqrt{Re_{\infty}}$.

CPBL C obtained from interacting boundary layer calculation.

QW Heat transfer coefficient at the wall.

STAN Stanton number.

STRINT Intermittency parameter in streamwise direction.

CFX Scaled skin friction coefficient, $c_f \sqrt{Re_{\infty}}$.

Summary of Convergence History

INTRAC Interaction global iteration counter.

DDTMAX Maximum change in DT.

RMSDT Root mean square change in DT.

SMDT Streamwise location where DDTMAX occurs.

DUEMAX Maximum change in UE.

RMSUE Root mean square change in UE.

SMUE Streamwise location for maximum change in UE.

DSFMAX Maximum change in perturbation stream function, f.

DFMAX Maximum change in velocity ratio, F.

DGMAX Maximum change in total enthalpy ratio, G.

Brief Description of Files

The following files are used to write information for plotting, restart, and interaction purposes.

<u>Unit Number</u>	<u>Purpose</u>
8	Write velocity and temperature profiles to be used for plotting purposes later on (TURBID).
9	Write stream function profile to be used for plotting purposes later on (TURBID).
10	Write eddy viscosity coefficient profile to be used for plotting purposes later on (TURBID).
12	Read information for restart run (TURBID).

13	Write information for later restart (WR13).
14	Write the profiles in inverse variables from a direct boundary layer run at the last streamwise station (CONVRT).
17	Write the weak interaction solution from a direct boundary layer run for use as a reference solution (TURBID).
18	Direct access file to store information for windward differencing scheme (TURBID).
22	Write station quantities for Tektronics plotting (WR22).

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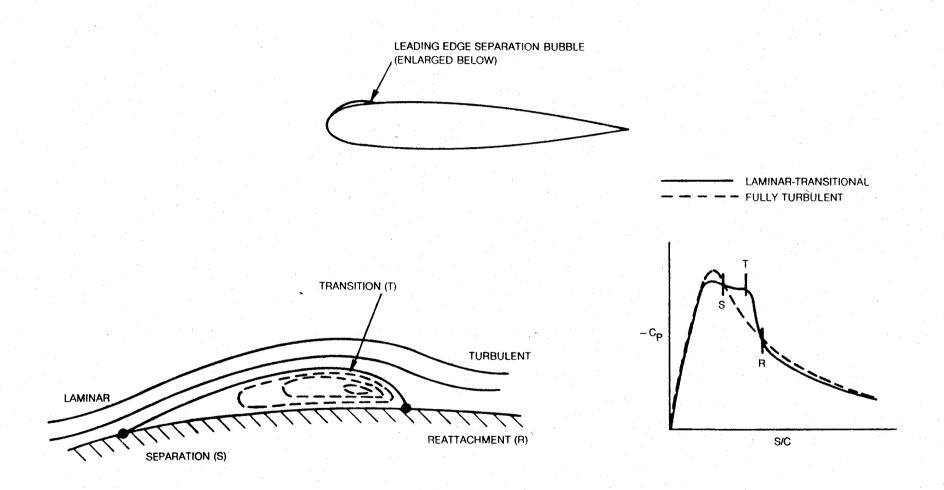


Fig. 1 Schematic diagram of airfoil laminar-transitional separation bubble and pressure distribution

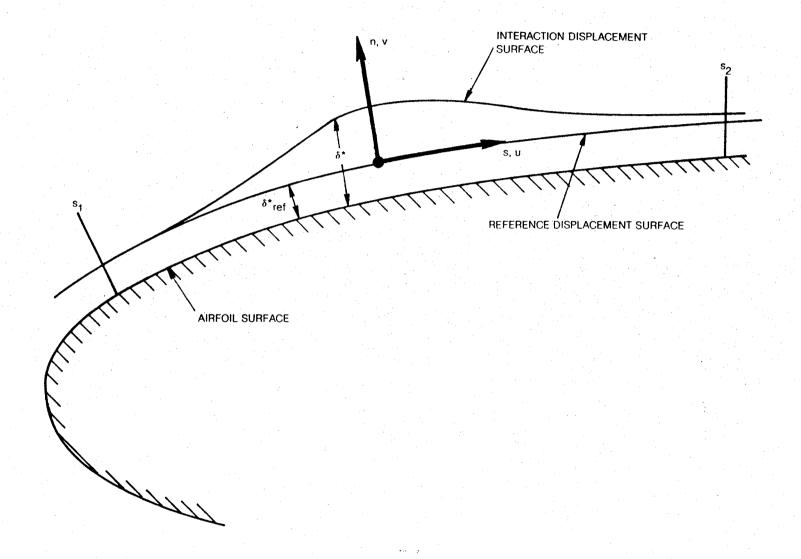


Fig. 2 Local interaction region coordinate system

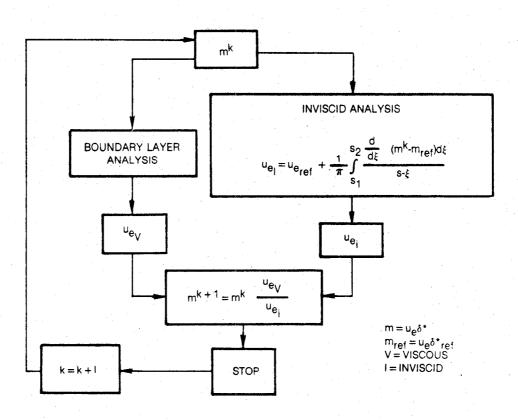


Fig. 3 Inviscid-viscous interaction procedure

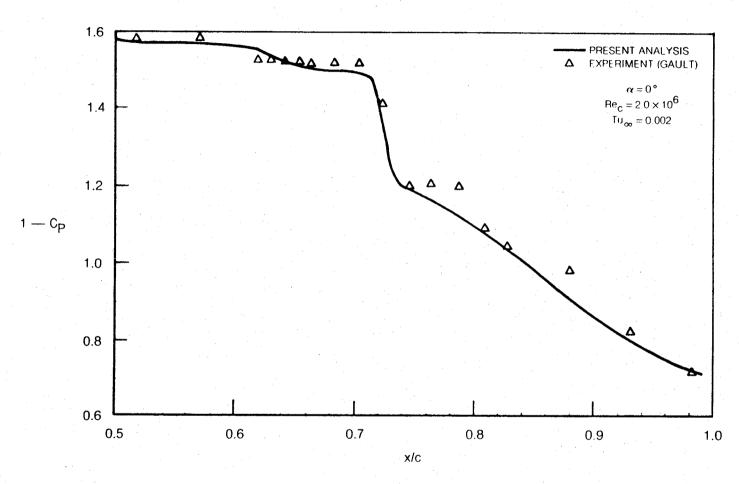


Fig. 5 Predicted results for NACA 66₃-018 airfoil.
(a) Pressure distribution.

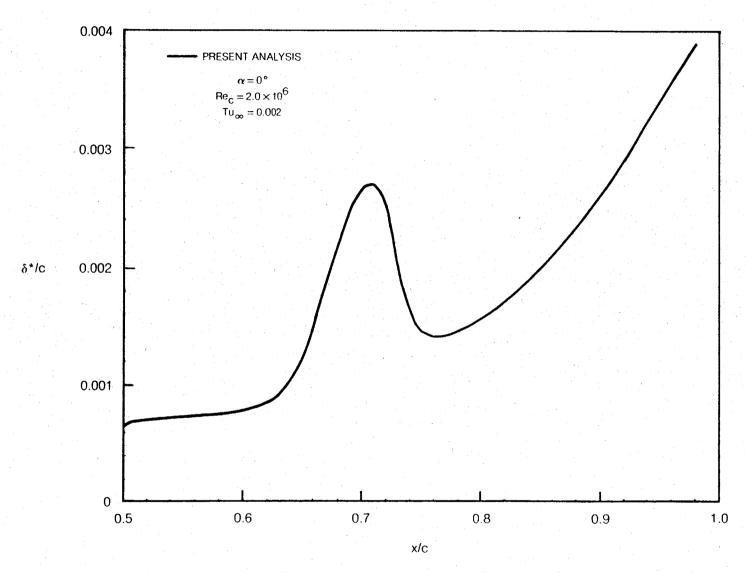


Fig. 5 Predicted results for NACA 663-018 airfoil (b) Displacement thickness.

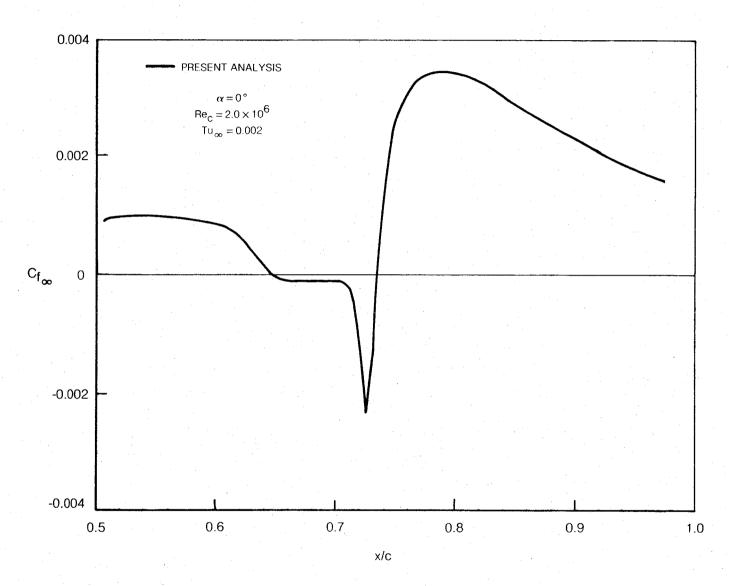


Fig. 5 Predicted results for NACA 66₃-018 airfoil. (c) Skin friction.

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IVT2=0,
ISMOTH=0,
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ITEK=0,
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IFILET=0,
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  XTZ= 9.34,
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   YSTING=0..
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حاجر إستعاد

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              1.2978
```

INVERSE RUN CASE, REC=2.*10**6 -- .2% TURBULENCE

I .	X0 -	YO	50	CPO	DTO	TUO
123456789011234567890123456789012334	.004962 .004962 .0049929 .0049929 .0073191391391391391391391391391391391391391	.00000 .000000	004962 0004962 0004962 00199227 011913848 0125989991 0125989991 0125989991 0125989991 0125989991 0125989991 01259899999999999999999999999999999999999	1.0000 .783007 .193007 .193007 .10194116 .101942653337 .101942653337 .101942653337 .101942653337 .101942653337 .101942653337 .10194265337 .10194265337 .10194265337 .10194265337 .1019426533 .1019426533 .1019426533 .1019426533 .1019426533 .1019426533 .1019426533 .1019426533 .1019426533 .1019426533 .1019426533 .101942653 .1019426533 .101942653 .1019426533 .101942653 .1019	.00000 .00000	.002000 .002200 .00200 .002200 .002200 .002200 .002200 .002200 .00200 .00200 .00200
I	S 1	SMOOTH	VT INPL	JT VT		
1 2 3 4 5 6 7 8 9 10 11	.000000 .005000 .015000 .015000 .025000 .035000 .035000 .045000 .050000	.0203 .4258 .6997 .8443 .9274 .9771 1.0079 1.0233 1.0326 1.0418	75 47 67 83 11 70 16 10 20 10 10 10 10 10 10 10 10 10 10 10 10 10	019994 667394 715935 826788 928191 972494 911455 921564 931564 941618		

1.5		A55600	1 041445	1.061727
12 13 14		.055000 .060000 .065000	1.061665 1.071823	1 071761
13		•060000	1.011953	1.071781
14		•065000	1.082059	1.081836
15		.070000	1.092131	1.091890
16		-075000	1.100931	1.101914
17		000000	1 107108	1.106952
1.		• 000000	1.107170	1.111989
Τū		•005000	1.115503	1.111989
19		•090000	1.11/0//	1.117027
20		•095000	1.122055	1.117027
21		-100000	1.127091	1.117027 1.122065 1.127102
55		105000	1.132134	1.127102 1.132140 1.137177
55		110000	1.132134	1 1 2 7 1 7 7
23.		•110000	1.142230	1 1 4 7 7 7 1 6
2.4		-115000	1.142230	1.142215
25		.120000	1.147328	1.14/222
26		.125000	1.152390	1.152290
- 27		.130000	1.157037	1.152290 1.157327
28		.135000	1.160750	1.106952 1.111989 1.117027 1.122065 1.127102 1.1321477 1.1472215 1.1472215 1.157327 1.160772 1.1607712
2 ğ		140000	1.163807	1.160772 1.163712 1.166653
ັກດ໌		145000	1.166692	1.166653
. 30		150000	1 140504	1 160504
3.7		*150000 ·	1.107770	1.169594
32		122000	1.1(5)21	1.1/2222
. 33		•160000	1.175474	1.1/54/6
34		•165000	1.157037 1.160750 1.163807 1.166692 1.169596 1.172531 1.175474 1.178416 1.181356 1.184304 1.187267 1.190221 1.193029	1.117989 1.117027 1.1271002 1.13211477 1.13211477 1.1472215 1.157327 1.160772 1.166659 1.1695935 1.1754376 1.1784158 1.178458
35	**	.170000	1.181356	1.181358
36		175000	1.184304	1.184299
37		180000	1 187267	1.184299
36		185000	1 100221	1 100181
20		• 100000	1.190221	1 102121
39		.075000 .0850000 .0850000 .1050000 .11500000 .11500000 .115500000 .115500000 .115500000 .115500000 .115500000 .115500000 .115500000 .115500000 .115500000 .115500000 .115500000 .115500000 .115500000 .1155000000 .116000000 .117500000 .1180500000 .1180500000 .1180500000 .1180500000 .1180500000 .1180500000 .11805000000 .118050000000 .118050000000000000000000000000000000000	1.193029	1.132140 1.137175 1.1472520 1.1522297 1.1522297 1.1607772 1.1607772 1.1606594 1.1725376 1.1784358 1.1784358 1.184240 1.193515 1.193515 1.193515 1.1975695
40		.195000	1.195479	1-145515
41		•200000	1.197630	1.197590
42		·205000	1.199684	1.199665
43		-210000	1.201742	1.201740
44		-215000	1.203813	1.201740 1.203814 1.205889 1.207964 1.210039
45		- 220000	1.205888	1.205889
7,4		226000	1 207062	1 207064
. 40		• 223000	1.21002	1 210020
4 (.220000 .225000 .230000 .235000 .240000	1.210037	1.510034
48		235000	1.212123	1.0212114
49		·240000	1.214235	1.214189
-50		·245000	1.201742 1.203813 1.205888 1.207962 1.212123 1.212123 1.214235 1.218166 1.219425 1.220255 1.220266 1.221687 1.221687 1.222427 1.223173	1.212114 1.214189 1.216264 1.218338 1.219450
51		•250000	1.218166	1.218338
52		255000	1.219425	1.219450
53		-260000	1.220255	1.220195
54		265000	1.220066	1.220195 1.220940 1.221685 1.222429 1.223174 1.223919 1.224664
66		270000	1 221687	1 221685
22		275000	1 222427	1.222420
50		•275000	1.6222721	1.222424
51		• 280000	1.2231/3	1.2231/4
58		•285000	1.223917	1.223919
59		•290000	1.224656	1.224664
60		295000	1.225401	1.225408
61		300000	1.226190	1.226157
<u>د ۲</u>		305000	1.227063	1.227072
42		• 30,000	1 227070	1 227004
ڊو		•310000	1.224656 1.225401 1.226190 1.227063 1.227979 1.228899	1.225408 1.226157 1.227072 1.227986 1.228901
64		•315000	1.558844	1.559401
65		•320000	1.229816	1.229816
1111122222222233333333334444444445555555556666666666		11650000 11750000 11750000 11850000 11850000 119500000 20050000 2215000000 221500000 221500000 221500000 221500000 221500000 221500000 221500000 221500000 221500000 221500000 221500000 221500000 221500000 221500000 221500000 221500000 221500000 2215000000 2215000000 2215000000 22150000000000	1.01931 1.019093	1.0699827223345418990111.0111.0111.0111.0111.0111.0111.0
67		.330000	1.231645	1.231645
68		•33500Õ	1.231645 1.232561 1.233478 1.234389	1.232560
69		340000	1.233478	1.232560
76		345C00	1.234389	1.234380
5 Y		350000	1.235276	1 2 25 2 2 7
11		• 350000	1.4237410	1.234389 1.235287 1.236123
12		. 350000	1.236127	1.236123

77777778812345678899999999999999999999999999999999999	00000000000000000000000000000000000000	1.234799 1.2377930 1.238662 1.2387630 1.22481141 1.22411978 1.22441978 1.22441978 1.224457679 1.224457679 1.22465764 1.22465764 1.22465764 1.22465764 1.22465767 1.2246767 1.2246767 1.225528847 1.22552844 1.22552844 1.22552844 1.2255284 1.2255665 1.2255673 1.225567 1.2255773 1.2255773 1.225676 1.225676 1.225677 1.22663747 1.22663	112444456736621771617.6482579366237971093366911122444456762666666677764227222555657778898466534747478121122444466767673344362277112255555657778898466337474716112244447887471111112555556577788940653477776447886666666666666677776666666666
130 131 132 133	.645000 .650000 .655000	1.254932 1.250508 1.244107 1.235921	1.254630 1.254630 1.250926 1.244412 1.235776

134	134	•665000	1.227241	1.227141
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1885000 178 179 1890000 177 180 180 180 180 180 180 180 180 180 180	135	.670000	1.219083	1.218777
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	137	490000	1.204989	1.205087
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	138	690000	1.198164	1.198242
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1885000 178 179 1890000 177 180 180 180 180 180 180 180 180 180 180	140	695000	1.185024	1.184814
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1885000 178 179 1890000 177 180 180 180 180 180 180 180 180 180 180	141		1.173836	1.173879
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1885000 178 179 1890000 177 180 180 180 180 180 180 180 180 180 180	143	•710000 715000	1.168411	1.168411
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	145	720000	1.157279	1.157267
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	147	•725000 •730000	1.151586	1.145863
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	148	•735000 740000	1.140062	1.140085
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	150	745000	1.128265	1.128264
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	151 152	•750000 •755000	1.122351	1.122354
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	153	.760000	1.110665	1.110672
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	155	770000	1.099088	1.099114
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	156 157	•775000 •780000	1.093336	1.093335
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	158	.785000	1.082406	1.082429
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1885000 178 179 1890000 177 180 180 180 180 180 180 180 180 180 180	160	795000	1.071959	1.071947
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1885000 178 179 1890000 177 180 180 180 180 180 180 180 180 180 180	161	- 805000	1.066647	1.066706
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1885000 178 179 1890000 177 180 180 180 180 180 180 180 180 180 180	163	-810000	1.055607	1.055577
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	165	.820000	1.044310	1.044363
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	166	.825000 .830000	1.038481	1.038445
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	168	835000	1.026614	1.026607
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	170	•845000 •845000	1.013343	1.013324
173 174 1865000 175 176 177 1870000 177 177 1870000 177 178 1880000 177 178 1880000 178 179 1890000 180 180 180 180 180 180 180 180 180	171	.850000 .855000	1.006183	1.006195
175	173	-860000	992778	992739
176	175	.870000	.980864	.980892
192 -955000 -880608 -880607	176 177	.875000 .880000	.974959 .969045	•974969 •969046
192 -955000 -880608 -880607	178	885000	.963178	.963149
192 -955000 -880608 -880607	180	.895C00	.951663	951657
192 -955000 -880608 -880607	181 182	•900000 •905000	•945938: •940152	•945912 •940166
192 -955000 -880608 -880607	183	.910000	.934162	•934235 937878
192 -955000 -880608 -880607	185	.920000	921514	921521
192 -955000 -880608 -880607	186 187	•925000 •930000	.915132 .908913	•915164 •908807
192 _955000 _880608 _880607	188	935000	•903038 807305	903036
192 _955000 _880608 _880607	190	945000	891813	891822
193 •960000 •874906 •874913 194 •965000 •869062 •869127	191 192	•950000 •955000	.886226 .880608	.886215 .880607
	193 194	.960000 .965000	•874906	.874913 .869127

195 196 197 198 199	•970000 •975000 •980000 •985000 •990000	.863087 .857375 .853250 .852002 .852229	•863341 •857555 •852232 •852232
I	S 1	SMOOTH PMF	INPUT PMF
123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012	.00000 .0150000 .0150000 .0200000 .0250000 .03500000 .03500000 .03500000 .04500000 .05500000 .06500000 .075000000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .075000000 .075000000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .07500000 .0750000000 .075000000 .075000000 .075000000 .0750000000000	.000000 .000000 .000000 .000000 .000000 .000000	-000000 -000000 -000000 -000000 -000000 -000000

	The second second		
6.3	310000	00000	000000
23	• 260000	•000000	•000000
54	-265000	•000000	•000000
55	• 270000 ·	•000000	•000000
56	•275000	•000000	•000000
5.7	.270000 .275000 .280000	•000000	.000000
53 54 55 56 57 58 59 60	.265000 .270000 .275000 .285000 .295000 .295000 .300000	.000000	.000000
20	*200000		.000000
29	• 290000	•000000	
οŪ	•295000	•000000	•000000
61 62 63	•300000	•000000	.000000
62	.305000	•000000	•000000
63	.310000	•000000	•000000
64	-315000	•000000	•000000
65	.310000 .315000 .320000 .325000 .330000	.000000	.000000
66	325000	.000000	.000000
4.7	320000	.000000	.000000
01	• 330000		
00	.290000 .295000 .300000 .310000 .315000 .320000 .325000 .335000 .345000	•000000	•000000
69	•340000	•000000	•000000
70	•345000	•000000	•000000
71	•350000	•000000	•000000
72	·355000	.000000	.000000
73	-360000	.000000	•000000
74	365000	.000000	.000000
75	370000	.000000	.000000
666789012345678901234567888888888888888888888888888888888888	.345000 .355000 .355000 .365000 .365000 .375000	.000000	.000000
10	.375000 .380000	•000000	-000000
46	• 300000	•000000	.000000
78	.385000 .390000	•000000	•000000
79		•00000	•000000
80	•395000	•000000	•000000
81	• 400000	•000000	.000000
82	405000	•000000	•000000
หัว	410000 415000 420000 425000 435000 440000	.000000	.000000
84	415000	.000000	.000000
9.5	420000	.000000	.000000
0.7	425000	•000000	
00	• 425000	•000000	•000000
87	•430000	•000000	•000000
88	·435000	•000000	•000000
. 89	• 440000	•000000	•000000
90		•000000	•000000
89 90 91 92 93	450000	•000000	.000000
92	.455000	•000000	.000000
93	•460000	•000000	.000000
94	465000	.000000	.000000
ás	- 47 0000	.000000	.000000
95 96	475000	.000000	.000000
97	.475000 .480000		
91	• 400000	•000000	•000000
98	.485 000	•000000	•000000
99	•490000	•000000	•000000
100	•495COO	•000000	•000000
101	•500000	•000000	.000000
102	-505000	•000000	•000000
103	-510000	•000000	.000000
104	515000	.000000	.000000
105	520000	.000000	.000000
	• J & U U U U	• 000000	
106	• 525600	•000000	•000000
107	• 5 3 0 0 0 0	•000000	•000000
108	• 235000	•000000	•000000
109	• 540000	•000000	•000000
110	•545000	•000000	.000000
111	•550000	•000000	.000000
111 112	.555000	.000000	•000000
113	• 49000 • 495000 • 505000 • 515000 • 515000 • 525000 • 530000 • 545000 • 545000 • 555000 • 55000 • 55000 • 55000 • 55000 • 56000	.000000	.000000
		•00000	•000000

	.565000 .5770000 .5775000 .585000 .585000 .595000 .605000 .615000 .625000 .635000	00000	000000
114	• 565000	.000000	•000000
115	570000	.000000	.00000 .00000 .00000 .00000 .00000
**/	• 5 7 0 0 0 0	*000000	• 000000
110	• > 1 > 0 0 0	• 000000	• 000000
116	-580000	-000000	_000000
117 118	• 60 60 00	•000000	***************************************
110	• 202000	• 000000	• 000000
119	~590000	-000000	_000000
136	* 60 6000	-000000	*********
120	•343000	• 000000	• 000000
121	- 600000	- 000000	_0000000
155	705000	• 000000	000000
122	• 605000	• 000000	• 000000
123	-610000	-000000	_000000
134	415000	000000	000000
124	• 012000	• 000000	•000000
125	.615000 .620000 .625000 .630000	• •000000	•000000
136	435000	000000	000000
170	•025000	• 000000	• 000000
127	•630000	•000000	•000000
120	635000	000000	000000
170	• 632000	• 000000	•000000
129	.640000	_000000	•000000
130	645000	000000	. 000000
130	•042000	• 000000	• 000000
131	•650000	•000000	•000000
121234567890112345678901133456789011334567890113345678901133456789011334567890113456789000000000000000000000000000000000000	.650000 .655000	000000	-000000
132	•033000	• 00000	• 000000
133	.660000	•000000	•000000
134	.665000	000000	.000000
137	• 00 00 00	• 000000	• 000000
135	.670000	• 000000	•000000
136	.675000 .680000	- 000 000	-000000
+ 30	•013000	• 000 000	• 000000
137	•680000	•000000	•000000
138	•685000	- 000000	_000000
133	•00000	•000000	***********
139	.690000	•000000	• 000000
140	- 695000	~000000	_000000
1	90000		******
141	.695000 .695000 .700000	• 000000	• 000000
142 143 144	.705000 .705000 .710000	_000000	_000000
1.75	710000	********	000000
143	• / 10000	• 000000	•000000
144	-715000	-000000	•000000
145	720000	000000	.000000
177	• 120000	• 000000	• 000000
146	• 725000	•000000	•000000
147 148	730000	. 000000	-000000
171	• 130000	•000000	• 000000
148	• 735000	• 000000	•000000
149	-740000	~000 00 0	-000000
îió	745000	000000	000000
120	• 745000	• 000000	•000000
151	.75 0000	-000000	_000000
149 150 1512 1523 1556 1567 1567 1590	715000 720000 725000 735000 735000 745000 755000 756000 765000 775000 775000	000000	000000
127	• 755000	•000000	• 000000
153	• 760000	•000000	•000000
154	765000	- 000000	-000000
177	. 703000	• 000000	•00000
122	• / / 0000	•000000	•000000
156	. 775000	~000000	_000000
163	70000	********	********
121	• /80000	•000000	•000000
158	~7 85000	-000000	_000000
îñă	700000	000000	000000
アンカ	• 790000	•000000	•000000
160	-795000	-000000	-000000
1 4 1	900000	000000	000000
TOT	• 000000	• 000000	• 000000
162	. 805000	•000000	•000000
163	810000	ññññññ	. 000000
161 162 163	• O F O O O	• 000000	• 200000
164	.815000	•000000	•000000
165	เลือดกัดกั	- 000000	-000000
107	779000 785000 790000 895000 805000 815000 815000 825000 825000 835000 835000	.000000 .000000 .000000 .000000 .000000 .000000	• 000000
166	.825COO	•000000	•000000
167	830000	.000000	-000000
177	• 030000	• 000000	• 000000
TOR	•835000	• 000000	• 000000
169	-840000	-000000	-000000
174	945000	*******	000000
110	•042000	• 000000	• • • • • • • • • • • • • • • • • • • •
171	.845000 .850000	•000000	.000000
175	PEEDON	7000000	000000
116	855000	• 000000	•000000
165 166 167 168 169 170 171 172 173 174	860000	000000 000000 000000 000000 000000 00000	•000000
17%	865000	000000	.000000
114	865000	• 000000	• 000000

See See

175	.870000	.000000	.000000
176	.875000	•000000	•000000
177	•880000	•000000	•000000
178	.885COO	.000000	.000000
179	890000		
		•000000	•000000
180	. 895000	•000000	•000000
181	•900000	.000000	•000000
182	905000	.000000	.000000
183	910000	.000000	.000000
184	•915000	•000000	•000000
185	•920000	•000000	•000000
186	•925000	•000000	.000000
187	930000	•000000	.000000
188	•935000	.000000	•000000
189	•940000	•000000	•000000
190	•945000	.000000	.000000
Ī91	950000	.000000	.000000
192	•955000	•000000	.000000
193	•960000	•000000	•000000
194	•965000	•000000	•000000
195	•970000	.000000	-000000
196	.975000	.000000	•000000
197	•980000	•000000	000000
198	•985000	•000000	•000000
199	990000	.000000	.000000
* * * * * * * * * * * * * * * * * * * *	• ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	• • • • • • • • • • • • • • • • • • • •	• 000000

SMOOTHED REFERENCE SOLUTION ON COMPUTATIONAL MESH

1 .	51	XB	YB	VT	PMFB	TUB
1	.00000	.00000	.00000	.02036	.00000	.00200
ζ.	• 00 500	• 00500	•00000	- 42588	.00000	.00200
3	•01000	.01000	•00000	•69975	•00000	•00200
5	•01500 •02000	•01500	•00000	84438	• 00000	•00200
_	•02500	•02000 •02500	•00000	•92741	•00000	•00200
6	.03000	•02900	-00000 -00000	.97717 1.00792	•00000	•00200 •00200
8	•03500	•03500	.00000	1.02332	.00000	.00200
ğ.	04000	04000	.00000	1.03270	.00000	.00200
1ó	04500	04500	.00000	1.04181	.00000	.00200
īĭ	05000	.05000	.00000	1.05159	.00000	.00200
ĨŽ.	05500	• 05500	.00000	1.06166	.00000	.00200
13	• 06000	• 06000	.00000	1.07182	.00000	.00200
14	•06500	•06500	.00000	1.08206	.00000	.00200
15	• 07000	• 07000	•00000	1.09213	•00000	•00200
16	•07500	•07500	•00000	1.10093	•00000	.00200
1.7	.08000	•08000	•00000	1.10720	• 00000	•00200
18	.08500	.08500	•00000	1.11221	•00000	•00200
19	•09000	•09000	•00000	1.11708	•00000	•00200
20	• 09500	• 09500	•00000	1.12206	•00000	•00200
21	10000	-10000	•00000	1.12709	• 00000	•00200
22 23	•10500 •11000	.10500 .11000	.00000	1.13213	.00000	• 00 200
24	.11500	.11500	.00000	1.14223	.00000	.00200 .00200
25	12000	.12000	.00000	1.14733	.00000	.00200
26	•12500	12500	.00000	1.15239	.00000	.00200
. 27	•13000	13000	.00000	1.15704	.00000	.00200
28	•13500	.13500	.00000	1.16075	.00000	•0CZC0
29	-14000	14000	-00000	1.16381	.00000	100200

30	-14500	.14500	.00000	1.16669	•00000	•00200
31 32	•15000 •15500	•15000 •15500	.00000 .00000	1.16960 1.17253	•00000 •00000	.00200 .00200
33	•16000	.16000	.00000	1.17547	•00000	.00200
34	• 16500	.16500 .17000	.00000 .00000	1.17842 1.18136	.00000 .00000	.00200 .00200
35 36	•17000 •17500	17500	.00000	1.18430	.00000	.00200
37	.18000	.18000	.00000	1.18727	•00000	•0C200
38	•18500 •19000	.18500 .19000	.00000	1.19022 1.19303	.00000 .00000	.00200 .00200
40	19500	19500	• 00 0 0 0	1.19548	.00000	.00200
41	• 20000	· 20000	•00000	1.19763 1.19968	.00000	•00200 •00200
42	.20500 .21000	.20500 .21000	.00000 .00000	1.20174	.00000	.00200
44	21500	.21500	.00000	1.20174	.00000	•00200
45	•22000 •22500	•22000 •22500	.00000 .00000	1.20589 1.20796	.00000 .00000	.00200 .00200
46 47	.23000	.23000	.00000	1.21004	.00000	.00200
48	.23500	• 23500	•00000	1.21212	•00000	•00200
49 50	•24000 •24500	•24000 •24500	.00000	1.21423 1.21633	•00000	•00200 •00200
51	.25000	.25000	.00000	1.21817	.00000	.00200
52	• 25500	• 25500	.00000	1.21943	.00000	.00200 .00200
53	• 26000 • 26500	.26000 .26500	.00000	1.22097	.00000	.00200
55	.27000	.27000	.00000	1.22169	•00000	•00200
56 57	•27500 •28000	.27500 .28000	.00000 .00000	1.22243	.00000	.00200 .00200
58	.28500	28500	.00000	1.22317	.00000	.00200
59	-29000	- 29000	.00000 .00000	1.22466	.00000 .00000	•00200
60 61	•29500 •30000	• 29500 • 30000	.00000	1.22540	.00000	.00200
62	-30500	.30500	•00000	1.22706	.00000	.00200
63 64	•31000 •31500	•31000 •31500	.00000 .00000	1.22798	.00000	.00200 .00200
65	32000	.32000	.00000	1.22982	.00000	.0C200
66	• 32500	•32500 •33000	.00000 .00000	1.23073 1.23165	•00000 •00000	.00200
67 68	•33000 •33500	•33500	.00000	1.23165	.00000	.00200
69	.34000	.34000	.00000	1.23348	•00000	.00200
. 70 71	• 34500 • 35000	•34500 •35000	•00000	1.23439	.00000 .00000	.00200 .00200
72	35500	35500	.00000	1.23613	.00000	.00200
73	•36000	• 36000	•00000	1.23696 1.23780	.00000 .00000	.00200 .00200
74 75.	•36500 •37000	•36500 •37000	.00000 .00000	1-23863	.00000	.00200
76	.37500	.37500	.00000	1.23947	.00000	.00200
77 78	•38000 •38500	.38000 .38500	•00000	1.24030 1.24114	.00000	.00200 .00200
79	.39000	39000	.00000	1.24198	.00000	.00200
80	.39500	• 39500	•00000	1.24280	•00000	•00200
81 82	.40000 .40500	•40000 •40500	.00000 .00000	1.24358	.00000 .00000	.00200 .00200
83	.41000	.41000	.00000	1.24506	.00000	.00200
84	•41500 43000	• 41500 63000	-00000 -00000	1.24579	.00000 .00000	.00200 .00200
85 86	.42000 .42500	•42000 •42500	•00000	1.24653 1.24727	.00000	.00200
87	.43000	.43000	.00000	1.24800	.00000	.00200
88 89	•43500 •44000	•43500 •44000	.00000	1.24874 1.24948	.00000 .00000	•00200 •00200
90	• 44500	.44500	.00000	1.25022	.00000	00200

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91	• 45000	• 45000	.00000	1.25096	•00000	•00200
92	• 45500	• 45500	•00000	1.25167	•00000	•00200
93	•46000	• 46000	•00000	1.25229 1.25284	•00000	•00200
94	• 46500	• 46500	•00000	1.25284	•00000	•00200 •00200
95	• 47000	•47000	•00000		.00000 .00000	.00200
96	• 47500	• 47500	.00000	1.25390	.00000	.00200
97 98	•48000 •48500	• 48000 • 48500	.00000	1.25496	.00000	.00200
99	49000	49000	.00000	1.25549	.00000	.00200
100	49500	49500	.00000	1.25603	.00000	.00200
ioi	50000	.50000	.00000	1.25658	.00000	.00200
102	.50500	.50500	.00000	1.25716	•00000	•00200
103	•51000	•51000	.00000	1.25774	.00000	.00200
104	•51500	•51500	•00000	1.25832	•00000	•00200
105	.52000	• 52000	.00000	1.25890	• 00000	•00200
106	•52500	•52500	•00000	1.25949	• 00000	•00200
107	• 5 3000	• 5 3000	• 00000	1.26007	•00000 •00000	•00200 •00200
108	• 53500	• 53500	•00000	1.26066 1.26123	.00000	.00200
109 110	•54000 •54500	•54000 •54500	.00000	1.26171	.00000	.00200
iii	55000	55000	.00000	1.26209	.00000	.00200
	55500	55500	.00000	1.26242	.00000	.00200
112	-56000	-56000	.00000	1.26275	.00000	.00200
114	• 56500	•56500	.00000	1.26308	• 00000	•00200
115	•57000	•57000	.00000	1.26341	•00000	•00200
116	•57500	• 57500	•00000	1.26375	•00000	•00200
117	• 58000	• 58000 • 58000	.00000	1.26408 1.26441	•00000 •00000	.00200
118	•58500 •59000	•58500 •59000	.00000	1.26474	.00000	.00200
120	•59500	•59500	.00000	1.26511	.00000	.00200
121	60000	60000	.00000	1.26558	.00000	.00200
122	.60500	60500	.00000	1.26614	.00000	.00200
123	.61000	.61000	•00000	1.26677	.00000	.00200
124	•61500	•61500	.00000	1.26733	• 00000	•00200
125	•62000	•62000	•00000	1.26725	• 00000	•00200
126	•62500	•62500	• 00000	1.26587	.00000 .00000	.00200
127 128	•63000 •63500	•63000 •63500	.00000 .00000	1.26379 1.26137	.00000	.00200
129	.64000	64000	.00000	1.25842	.00000	.00200
13.ó	64500	64500	.00000	1.25493	.00000	.00200
131	65000	65000	.00000	1.25051	.00000	.00200
132	.65500	•65500	•00000	1.24411	•00000	•0CZ00
133	•66000	•66000	•00000	1.23592	•00000	•00200
134	. 66500	•66500	• 00000	1.22724	•00000	•00200
135	•67000	•67000	•00000	1.21908	.00000 .00000	.00200 .00200
136 137	.67500 .68000	•67500 •68000	.00000 .00000	1.20499	.00000	.00200
138	-68500	68500	.00000	1.19816	.00000	.00200
139	69000	.69000	.00000	1.19140	.00000	.00200
140	69500	69500	.00000	1.18502	.00000	.00200
141	.70000	.70000	.00000	1.17928	•00000	•00200
142	• 705 00	• 70500	•00000	1.17384	•00000	•00200
143	• 71000	•71000	•00000	1.16841	•00000	•00200
144	•71500	•71500 73000	•00000	1.16291 1.15728	•00000 •00000	•00200 •00200
146	•72000 •72500	•72000 • 7 2500	.00000	1.15159	.00000	.00200
147	73000	73000	.00000	1.14586	.00000	.00200
148	73500	.73500	.00000	1.14006	.00000	.00200
149	.74000	.74000	.00000	1.13418	.00000	.00200
150	• 74500	. 74500	.00000	1.12826	•00000	.00200
151	• 75000	• 75000	•00000	1.12235	•00000	•00200

152	-75500	• 75500	.00000	1.11648	•00000	.00200
153	•76000 •76500	•76000 •76500	•00000	1.11067 1.10488	.00000 .00000	.00200 .00200
155	77000	.77000	.00000	1.09909	.00000	.0C200
156	.77500	• 77500	•00000	1.09334	• 00000	•00200
157 158	•78000 •78500	.78000 .78500	•00000 •00000	1.08775 1.08241	•00000 •00000	.00200 .00200
159	79000	79000	.00000	1.07718	.00000	•00200
160	.79500	.79500	.00000	1.07196	.00000	.00200
161	•80000	-80000	.00000	1.06665	.00000	•00200
162 163	.80500 .81000	.80500 .81000	.00000 .00000	1.06117 1.05561	•00000 •00000	•00200
164	81500	81500	.00000	1.05000	-00000	.00200
165	.82000	.82000	•00000	1.04431	.00000	.00200
166	•82500 ·	•82500 83000	•00000	1.03848	•00000	•00200
167 168	.83000 .83500	.83000 .83500	•00000	1.03260 1.02661	.00000 .00000	•00200 •00200
169	.84000	84000	.00000	1.02026	.00000	.00200
170	·84500	84500	•00000	1.01334	.00000	.00200
171 172	.85000 .85500	•85000° •85500	.00000 .00000	1.00618	.00000 .00000	.00200 .00200
173	86000	86000	.00000	99278	.00000	.00200
174	.86500	86500	.00000	.98676	.00000	•00200
175 176	•87000 87500	• 8 7 00 0	•00000	•98086	•00000	•00200
177	.87500 .88000	.87500 .88000	•00000 •00000	•97496 •96905	•00000 •00000	•00200 •00200
178	.88500	88500	.00000	96318	.00000	.00200
179	.89000	.89000	.00000	•95740	.00000	.00200
180 181	.89500 .90000	•89500 •90000	.00000	•95166 •94594	.00000 .00000	•00200 •00200
182	90500	90500	.00000	94015	.00000	.00200
183	•91000	•91000	.00000	.93416	.00000	•00200
184	•91500	•91500	•00000	•92790	• 00000	•00200
185 186	•92000 •92500	•92000 •92500	.00000 .00000	•92151 •91513	•00000 •00000	•00200 •00200
187	•93000	.93000	.00000	.90891	.00000	.00200
188	•93500	•93500	•00000	•90304	• 00000	.00200
189 190	•94000 •94500	•94000 •94500	•00000 •00000	.89740 .89181	•00000 •00000	.00200 .00200
191	95000	95000	.00000	.88623	.00000	.00200
192	•95500	95500	.00000	.88061	.00000	.00200
193 194	•96000 •96500	•96000 •96500	•00000	•87491	-00000	•00200
195	97000	•97000	•00000 •00000	•86906 •86309	•00000 •00000	•00200 •00200
196	. 9750ŏ	97500	.00000	.85738	.00000	.00200
197	•98000	• 97960	•00000	.85325	.00000	•00200
198 199	•98500 •99000	•97960 •97960	•00000	•85200 •85223	•00000 •00000	•00200 •00200
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*** STREAMWISE LOCATIONS OF BOUNDARY LAYER CALCULATION, BODY RADIUS, FROM SUBROUTINE XBLGRD ***
                               XOCBL
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                            .78500000E+00
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       .79000000E+00
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T(I), I=1, ISTOP
-20361118E-01
                    ** TANGENTIAL SURFACE VELOCITY .42587502E+00 .69974665E+00
                                                                .84438338E+00
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.11850243E+01
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.11223511E+01
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INITIAL GUESS ON PMF
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INTERPOLATED PMF DISTRIBUTION FROM INITIAL GUESS .11667000E+01 .11044275E+01 .11077050E+01
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*** INITIAL PROFILES ***

N	ETA(N)	F1(N)	SF1(N)	G1(N)	T(N)
12345678901234567890123456789012	.00000E+00 9.26311E-04 1.93599E-03 3.03654E-03 4.23614E-03 5.54370E-03 8.52246E-02 1.20615E-02 1.4015E-02 1.4063E-02 1.4063E-02 1.4063E-02 1.4063E-02 1.4019E-02 2.7126E-02 2.7126E-02 2.7126E-02 2.7126E-02 2.7126E-02 2.7126E-02 3.42491E-02 3.42491E-02 3.42491E-02 3.42491E-02 3.42491E-02 3.426274E-02 4.73902E-02 4.73902E-02 5.82402E-02 7.84593E-02 8.64470E-02 1.14988E-01 1.14988E-01 1.26263E-01 1.38553E-01	.00000E+00 5.77794E-04 1.20759E-03 1.89376E-03 2.64166E-03 3.45672E-03 4.34289E-03 6.36769E-03 8.7692E-03 1.01246E-02 1.3246E-02 1.3246E-02 1.3246E-02 1.3903E-02 2.37962E-02 2.37962E-02 2.4419E-02 2.570561E-02 3.7962E-02 2.64702E-02 3.99820E-02 2.4413E-02 2.57056E-02 3.99820E-02 3.99820E-02 4.4132E-02 3.99820E-02 4.4137E-02 3.99828E-02 3.99828E-02 4.110378E-02 5.35726E-02 6.47889E-02 7.110378E-02 8.55193E-02	.00000E+00 6.23002E+04 1.30132E-03 2.03978E-03 2.84364E-03 3.71857E-03 5.70681E-03 6.83401E-03 9.39359E-02 1.241377E-02 1.599406E-02 2.21.57937E-02 2.25937E-02 2.	1.00000E+00 1.000000E+00 1.0000000000000000000000000000000000	1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00050E+00
32 33 35 36 37 38	1.38553E-01 1.51949E-01 1.66551E-01 1.82467E-01 1.99815E-01 2.18725E-01 2.39336E-01	8.55193E-02 9.36899E-02 1.02576E-01 1.12237E-01 1.22740E-01 1.34152E-01 1.46550E-01	8.58803E-02 9.34132E-02 1.01471E-01 1.10073E-01 1.19235E-01 1.28968E-01 1.39277E-01	9.9996E-01 9.99995E-01 9.99995E-01 9.99995E-01 9.99994E-01	1.00050E+00 1.00050E+00 1.00050E+00 1.00049E+00 1.00049E+00 1.00049E+00
39 40 41 42 43 44	2.61803E-01 2.86292E-01 3.12984E-01 3.42079E-01 3.73792E-01 4.08360E-01 4.46039E-01	1.60013E-01 1.74626E-01 1.90480E-01 2.07669E-01 2.26293E-01 2.46457E-01 2.68264E-01	1.50158E-01 1.6159E-01 1.73573E-01 1.86037E-01 1.98932E-01 2.12170E-01 2.25637E-01	9.9993E-01 9.9993E-01 9.9993E-01 9.9993E-01 9.9993E-01	1.00049E+00 1.00048E+00 1.00048E+00 1.00047E+00 1.00047E+00 1.00046E+00
46 47 48 50 51 52	4.87109E-01 5.31875E-01 5.80670E-01 6.33856E-01 6.91830E-01 7.55021E-01 8.23899E-01	2.91822E-01 3.17235E-01 3.44603E-01 3.74012E-01 4.05535E-01 4.39216E-01 4.75062E-01	2.39185E-01 2.52621E-01 2.65709E-01 2.78154E-01 2.89602E-01 2.99631E-01 3.07750E-01	9.99993E-01 9.99994E-01 9.99995E-01 9.99996E-01 9.9999E-01 9.9999E-01	1.00046E+00 1.00045E+00 1.00044E+00 1.00043E+00 1.00041E+00 1.00039E+00
53 54 55 56 57	8.98976E-01 9.80810E-01 1.07001E+00 1.16724E+00 1.27321E+00	5.13027E-01 5.52996E-01 5.94762E-01 6.39001E-01 6.82247E-01	3.13398E-01 3.15959E-01 3.14780E-01 3.09208E-01 2.98653E-01	1.00000E+00 1.000C0E+00 1.000C1E+00 1.000C1E+00	1.00037E+00 1.00036E+00 1.00033E+00 1.00031E+00 1.00028E+00

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2.82674E-01
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2.34128E-01
2.02537E-01
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        1.38873E+00
                            7.26869E-01
7.71056E-01
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1.00023E+00
        1.51464E+00
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 60
        1.65189E+00
                            8.13824E-01
        1.80148E+00
                            8.54050E-01
8.90560E-01
                                                                    1.00003E+00
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 61
                                                1.67705E-01
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1.00010E+00
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        1.96454E+00
                                                1.31635E-01
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9.67800E-02
6.56618E-02
4.03469E-02
2.19190E-02
                            9.22255E-01
9.48295E-01
9.68280E-01
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1.00002E+00
 63
        2.14228E+00
        2.14228E+00
2.33601E+00
2.54717E+00
2.77735E+00
3.02823E+00
3.30170E+00
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 64
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                            9.82381E-01
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                                              -1.50122E-08

2.90561E-09

-1.13542E-09

-5.53753E-11

-3.32677E-10

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 83
                                              -2.80746E-10

-2.80964E-10

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 84
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        3.11197E+01
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 98
        4.39322E+01
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                                         SUMMARY OF CONVERGENCE HISTORY
                                                                                                                                                   DFMAX
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INTRAC
               DDTMAX
                                   RMSDT
                                                      SMDT
                                                                       DUEFAX
                                                                                           RMSUE
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                               .24873E-01
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                                                                    .97713E-01
                                                                                       .60667E-02
                                 * * *
                                         SUMMARY OF CONVERGENCE HISTORY
                                                                                                                                                   DFMAX
                                                                                                                                                                      DGMAX
                                                                                                              SMUE
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INTRAC
               DOTMAX
                                   RMSDT
                                                      SMDT
                                                                       DUEMAX
                                                                                           RMSUF
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           -.27173E+00
                               .95139E-02
                                                  •99000E+00 --45837E-01 .-25718E-02
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EDGE QUANTITIES IN VISMFK AT STATION M= 44
                           .04000°
                                              TREFD
                                                         = 530.00000
                                                                                      TREF
                                                                                                 =1562.50000
= 1.21747
      MREF
                 =
      REYREF = 2000000.0
                                              ME2
                                                                   .04870
                                                                                     UE2
TU2
                                              RHNE2
                                                                   99961
                                                                                                          .00200
      TE2
                  =1562.25889
                                                                                                           . 99988
                                              QE2
UE1
                                                                   .00346
                                                                                      MUE2
                                                                                                  ×
      RO2
                         1.00000
      MEI
                           .04880
                                                                 1.21979
                                                                                      TEI
                                                                                                  =1562.25605
                                                                 1.00000
                                                                                                          .00346
      RHOE1 =
                           .99961
                                              ŘŌĪ
                                                                                      QĒĪ
        MFK QUANTITIES IN VISMEK AT STATION M= 44
CLINE = 2.12629 ALINEN = .15269
                                                                                                          .09019
      ACLINF =
                                                                                      ALINFO =
      AIMFKN =
                                              AIMFKO =
                                                                   .12000
                                                                                      AZMEK =
                                                                                                          .50000
                           .12000
                                                                                      DELIN
                                                                                                         4.39527
                           .20000
                                              BLTHK
                                                        =
                                                                 6.44983
      A3MFK =
      DELTU2 =
                                              DELTU1 =
                                                                                      DTINC2 =
                                                                 6.45033
                         6.44983
                                                                                                         3.73176
                                              VEDGE
                                                                 -.01328
                                                                                      NDELTU =
      DTINC1 =
                         3.81392
                                                                                                           .00000
                                              PSILIN =
                                                                   .11757
                                                                                      PSI12N =
PSI21N =
      NINNER =
                                 57
      PDI110 =
                            .12668
                                              PS1120 =
                                                                   .00000
                                                                                                           .06090
                                                                   .00000
                                                                                                           .00011
                         .57419
6.45525
                                              PS132N =
                                                                                      EMFK
      PSI31N =
                                              RTHEAT = 251.29068
                                                                                      AZMA3N =
                                                                                                           •3000ō
      RTAU
                                                                                                                                                                                                               910.651
        .71500E+0C 11 .45421E+01 .45421E+01 -.31380E+00 -.31371E+00 .12175E+01 .4870ZE-01 .55330E+03 -.43160E-03***
PROFILES AT M= 44 \text{ S(M)} = R^{-1} 7.15000E = 01 \text{ INVRSE} = 1 PMF(M) = 0.000E =
                                                                                                            4.54211E+00 BETA(M)= -3.13798E-01
                                                                                                                                                               RHOMUR (N)
                                                                                                                                                                                       T(N)
                                                             F2(N)
                                                                                      SE2(N)
                                                                                                              G2(N)
                                                                                                                                      EPSBAR(N)
             ETA(N)
                                     YBL(N)
                                                              .00000E+00
                                                                                                                                     1.00000E+00
                                                                                                                                                             9.99892E-01
                                                                                                                                                                                     1.00047E+00
                                     .00000E+00
                                                                                      .00000E+00
                                                                                                             1.00000E+00
              .00000E+00
                                                                                                                                                                                     1.00047E+00
                                                                                                             1.00000E+00
                                                                                                                                     1.00000E+00
                                                                                                                                                             9.99892E-01
9.99892E-01
                                    2.44577E-06
                                                          -8.64058E-04
                                                                                  -3.00618E-03
            9.26311E-04
                                                                                                                                                                                      1.00047E+00
                                                                                  -6.25775E-03
            1.93599E-03
                                                          -1.79956E-03
                                                                                                             1.00000E+00
                                                                                                                                     1.00001E+00
                                    5.11166E-06
                                                                                                            1.00000E+00
                                                                                                                                     1.0000ZE+00
                                                                                                                                                             9.99892E-01
                                                                                                                                                                                      1.00047E+00
                                    8.01748E-06
                                                          -2.81174E-03
                                                                                  -9.77214E-03
            3.03654E-03
                                                                                                                                                                                     1.00047E+00
                                                                                                                                                             9.99892E-01
                                                                                                             1.00000E+00
                                                                                                                                     1.00004E+00
            4.23614E-03
5.54370E-03
                                    1.11848E-05
                                                          -3.90609E-03
                                                                                  -1.35675E-02
                                                                                  -1.76625E-02
-2.20766E-02
                                                                                                            1.00000E+00
                                    1.46372E-05
                                                          -5.08836E-03
                                                                                                                                     1.00008E+00
                                                                                                                                                             9.99892E-01
                                                                                                                                                                                     1.00047E+00
                                                                                                             1.00000E+00
                                                                                                                                                             9.99892E-01
9.99892E-01
                                                                                                                                                                                     1.00047E+00
                                                          -6.36448E-03
                                                                                                                                     1.00013E+00
            6.96895E-03
                                    1.84004E-05
                                                                                                                                                                                      1.00047E+00
            8.52246E-03
1.02158E-02
                                    2.25022E-05
2.69731E-05
                                                                                                             1.00000E+00
                                                                                                                                     1.00020E+00
                                                                                  -2.68292E-02
                                                                                                                                                             9.99892E-01
9.99892E-01
                                                                                                            1.00000E+00
                                                                                                                                     1.00029E+00
                                                          -9.22285E-03
-1.08176E-02
                                                                                  -3.19404E-02
-3.74296E-02
                                                                                                                                                                                     1.00047E+00
                                                                                                             1.00000E+00
                                                                                                                                     1.00042E+00
                                                                                                                                                                                     1.00047E+00
1.00047E+00
            1.20615E-02
                                    3.18465E-05
                                                                                                                                                             9.99892E-01
            1.40734E-02
                                    3.71584E-05
                                                                                  -4.33163E-02
                                                                                                             1.00000E+00
                                                                                                                                     1.00060E+00
                                                          -1.25313E-02
                                    4.29485E-05
                                                                                                            1.00000E+00
                                                          -1.43699E-02
                                                                                  -4.96189E-02
                                                                                                                                     1.00083E+00
                                                                                                                                                             9.99892E-01
9.99892E-01
                                                                                                                                                                                     1.00047E+00
   12
            1.62663E-02
                                                                                                                                    1.00113E+00
1.00153E+00
1.00204E+00
1.00270E+00
                                                                                  -5.63547E-02
                                                                                                                                                                                     1.00047E+00
1.00047E+00
                                    4.92596E-05
                                                                                                            1.00000E+00
            1.86566E-02
                                                          -1.63394E-02
                                    5.61387E-05
6.36370E-05
                                                          -1.84456E-02
-2.06933E-02
                                                                                  -6.35392E-02
-7.11855E-02
                                                                                                            1.00000E+00
                                                                                                                                                             9.9989ZE-01
            2.12620E-02
                                                                                                                                                                                     1.00047E+00
                                                                                                             1.00000E+00
                                                                                                                                                             9.99892E-01
9.99892E-01
            2.41019E-02
                                                                                                                                                                                     1.00047E+00
                                                                                                            1.00000E+00
            2.71973E-02
                                    7.18101E-05
                                                          -2.30870E-02
                                                                                  -7.93035E-02
                                                                                                                                                             9.99892E-01
9.99892E-01
9.99892E-01
                                                                                  -8.78993E-02
                                    8.07187E-05
9.04292E-05
                                                                                                             1.00000E+00
                                                                                                                                     1.00353E+00
                                                                                                                                                                                     1.00047E+00
            3.05714E-02
                                                          -2.56300E-02
                                                                                                                                                                                      1.00047E+00
                                                                                  -9.69740E-02
                                                                                                             1.00000E+00
                                                          -2.83245Ē-ÓŽ
                                                                                                                                     1.00460E+00
            3.42491E-02
            3.82579E-02
                                    1.01014E-04
1.12551E-04
1.25126E-04
                                                                                                                                                                                     1.00047E+00
                                                          -3.11712E-02
                                                                                  -1.06523E-01
                                                                                                             1.00000E+00
                                                                                                                                     1.00593E+00
   19012345567890123
                                                                                  -1.16536E-01
-1.26993E-01
                                                          -3.41691E-02
-3.73150E-02
                                                                                                                                     1.00757E+00
            4.26274E-02
                                                                                                            1.00000E+00
                                                                                                                                                             9.99892E-01
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                                                                                                                                     1.00959E+00
                                                                                                                                                             9.9989ZE-01
            4.73902E-02
            5.25816E-02
5.82402E-02
                                                                                                                                                                                      1.00047E+00
                                    1.38833E-04
1.53774E-04
                                                                                                                                     1.01201E+00
                                                                                                                                                             9.99892E-01
                                                          -4.06035E-02
                                                                                  -1.37867E-01
                                                                                                             1.00000E+00
                                                                                  -1.49121E-01
                                                                                                            1.00000E+00
                                                                                                                                                             9.99892E-01
                                                          -4.40265E-02
-4.75733E-02
                                                                                                                                     1.01488E+00
1.01820E+00
                                                                                                                                                                                     1.00047E+00
                                                                                                                                                             9.9989ZE-01
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            6.44082E-02
                                    1.70059E-04
                                                                                  -1.60709E-01
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                                                          -5.12298E-02
-5.49791E-02
                                                                                  -1.72574E-01
                                                                                                             1.00000E+00
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            7.11312E-02
                                    1.87810E-04
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9.99893E-01
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-1.96851E-01
                                                                                                             1.00000E+00
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                                    2.07159E-04
            7-84593E-02
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            8.64470E-02
                                    2.28249E-04
2.51237E-04
                                                          -5.88004E-02
                                                                                                             1.00000E+00
                                                                                                                                     1.03036E+00
                                                                                                                                     1.03467E+00
                                                          -6.26697E-02
            9.51535E-02
                                                                                  -2.09095E-01
                                                                                                             1.00000E+00
                                                                                                                                                             9.99893E-01
                                                                                                                                                                                     1.00047E+00
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                                                                                  -2.21277E-01
-2.33279E-01
                                                                                                                                     1.03867E+00
                                                                                                                                                             9.99893E-01
                                                                                                             1.00000E+00
            1.04644E-01
                                    2.76294E-04
                                                          -6.65582E-02
                                                                                                                                                                                     1.00047E+00
            1.14988E-01
                                                                                                             1.00000E+00
                                    3.03606E-04
3.33377E-04
                                                          -7.04317E-02
                                                                                                                                     1.04196E+00
                                                                                                                                                             9.99893E-01
                                                                                  -2.44959E-01
                                                                                                                                     1.04402E+00
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                                                                                                                                                                                      1.00047E+00
                                                          -7.42479E-02
-7.79516E-02
                                                                                                             1.00000E+00
            1.26263E-01
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                                                                                                                                     1.04417E+00
                                                                                                                                                             9.99893E-01
                                                                                                                                                                                     1.00047E+00
                                    3.65826E-04
                                                                                   -2.56143E-01
                                                                                                             1.00000E+00
                                                                                  -2.66598E-01
                                                                                                            1.00000E+00
            1.519498-01
                                    4.01196E-04
                                                          -8.14662E-02
                                                                                                                                     1.04158E+00
                                                                                                                                                             9.99893E-01
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                                                                                                                                                             9.99893E-01
   34
            1.66551E-01
                                    4.39750E-04
                                                          -8.46726E-02
                                                                                  -2.75980E-01
                                                                                                             1.00000E+00
                                                                                                                                     1.03634E+00
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                                    4.817738-04
                                                                                  -2.83726E-01
                                                                                                             1.00000E+00
                                                                                                                                     1.02901E+00
   35
            1.82467E-01
                                                                                                                                                             9.99893F-01
                                                          -8.73688E-02
                                                                                                                                                                                     1.00047E+00
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            Ī.99815Ē-01
                                    5.27578E-04
                                                          -8.91858F-02
                                                                                  -2.88842E-01
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3334444444444555555555555566666666666677777777	2.393334E-011 2.39333EE-011 2.61629849EE-011 2.61629849EE-011 2.61629849EE-011 3.4737960EE-011 4.87187960EE-011 4.8718796EE-011 4.8718796EE-011 4.8718796EE-011 4.8718796EE-011 4.8718796EE-011 4.8718796EE-011 4.8718796EE-011 4.8718796EE-011 4.8718796EE-011 4.8718796EE-011 4.8718796EE-011 4.8718796EE-011 4.8718796EE-011 4.8718796EE-011 4.8718796EE-011 4.8718796EE-000 4.8718796EE-000 4.8718796EE-000 4.8718796EE-000 4.8718796EE-000 4.8718796EE-000 4.8718796EE-000 4.8718796EE-000 4.8718796EE-000 4.8718796EE-000 4.8718796EE-000 4.8718796EE-001 4.8718796EE-00	 -8.93846E-022 -7.93740BE-022 -7.93740BE-022 -7.93740BE-022 -7.93740BE-022 -7.93740BE-022 -7.93740BE-022 -7.93766E-022 -7.93766E-022 -7.93766BE-022 -7.93766BE-022 -7.93766BE-011 -7.9376BE-011 -7.9376	-2.89388E-01 -2.6326E-01 -2.6326E-01 -2.6326E-01 -2.18576E-01 -2.18576E-01 -1.63021E-01 -1.63021E-02 -3.847507E-02 -3.847507E-02 -3.847507E-02 -3.847507E-01 -3.5193E-01 -3.5246E-01 -3.74774E-01 -3.74500E-02 -3.843774E-01 -7.74500E-01 -7.7536E-02 -3.8436E-01 -7.74500E-01 -7.7536E-02 -3.37940E-04 -3.38101E-06 -7.37242E-06 -7.37242E-06 -7.37940E-07 -1.39236E-07 -1.39236E-07 -1.39236E-07 -1.39236E-08 -7.393450E-08 -7.393450E-08 -7.39365E-08 -7.39365E-08 -7.39365E-08 -7.39365E-08 -7.39365E-08 -7.39365E-08 -7.393765E-08 -7.393765E-08 -7.393765E-08 -7.393765E-08 -7.393765E-08	9.99999E-01 9.99999E-01 9.99999E-01 9.99998E-01 9.99997E-01 9.99997E-01 9.99995E-01 9.99995E-01 9.99995E-01 9.99999E-01 9.99999E-01 1.000001E+00 1.000002E+00 1.000001E+00 1.000000E+00 1.00000E+00	1.0000000E+000 1.0000000EE+000 1.00000000EE+000 1.00000000EE+000 1.00000000EE+000 1.00000000EE+000 1.00000000EE+000 1.00000000EE+000 1.0000000EE+000 1.00000000EE+000 1.0000000EE+000	9.99893E-01 9.99893E-01 9.99893E-01 9.99893E-01 9.99893E-01 9.99893E-01 9.99893E-01 9.99893E-01 9.99893E-01 9.99893E-01 9.99893E-01 9.99893E-01 9.99893E-01 9.99894E-01 9.99896E-01 9.999906E-01 9.999906E-01 9.999912E-01 9.999912E-01 9.999912E-01 9.999912E-01 9.999912E-01 9.999912E-01 1.000000E+00	1.00047E+00 1.00047E+00 1.00047E+00 1.00047E+00 1.00047E+00 1.00047E+00 1.00047E+00 1.00047E+00 1.00047E+00 1.00047E+00 1.00044E+00 1.00044E+00 1.00044E+00 1.00044E+00 1.00044E+00 1.00044E+00 1.0004E+00 1.00039E+00 1.00003E+00 1.00003E+00 1.00003E+00 1.00000E+00

98 99 100 N	4.39322E+01 4.78870E+01 5.21978E+01 YN(N)	1.15942E-01 1.26379E-01 1.37756E-01 YPLUS(N)	1.00000E+00 1.00000E+00 1.00000E+00 DUDY(N)	-7.52281E-08 -7.74104E-08 .00000E+00 TAU(N)	1.00000E+00 1.00000E+00 1.00000E+00 DAMP(N)	1.00000E+00 1.00000E+00 1.00000E+00 FUN(N)	1.00000E+00 1.00000E+00 1.00000E+00 FMFK(N)	1.00000E+00 1.00000E+00 1.00000E+00 EPSBAR(N)
900N 1234567890112345678901200000000000000000000000000000000000	4.78878E+01 1.003778 1.003884E-0321 1.05884E-0321 1.058898E-0321 1.058898E-0311 1.068898E-0311 1.068898E-0321 1.068898E-0311 1.068898E-031 1.068	1.37-10 1.3	1.00000E+00 1.0000E+00 1.00000E+00 1.00000E+00 1.0000000000000000000000000000000000	-7.741C4E-08 0000E+00 13.011C6E-01 2.03235E-01 3.0111C6E-01 2.98268E-01 2.99547E-01 2.83800E-01 2.83800E-01 2.758807E-01 2.768387E-01 2.758807E-01 2.768387E-01 2.768387E-01 2.768387E-01 2.76883E-01 2.768883E-01 2.76888E-01	1.00000E+00 1.0000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.000000E+00 1.0000000000000000000000000000000000	1.0000E+00 0.000E+00 0.0000N(NE+0048140E+00481	1.00000E+00 1.00000E+00 1.00000E+00 0.00000E+00	1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.00002E+00 1.000029E+00 1.000029E+00 1.000029E+00 1.00060E+00 1.00060E+00 1.00060E+00 1.000579E+00 1.0005797E+00 1.00579FE+00 1.00579FE+00
46 47 48 49 51 55 55 55 55	1.81886E+00 1.98601E+00 2.16821E+00 2.36681E+00 2.581322E+00 3.07640E+00 3.366225E+00 3.99527E+00 4.35824E+00	8.75177E+01 1.05890E+02 1.27874E+02 1.54146E+02 1.54146E+02 2.58594E+02 2.58594E+02 3.25868E+02 3.39819E+02 3.28994E+02	1.75563E-01 1.95737E-01 2.17720E-01 2.41516E-01 2.66475E-01 3.12043E-01 3.25062E-01 3.254318E-01 3.04522E-01 2.63449E-01	1.63931E+00 2.01286E+00 2.46275E+00 3.00325E+00 3.63460E+00 4.32824E+00 5.00216E+00 5.50017E+00 5.60427E+00 5.12009E+00 4.03237E+00	1.0000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00	9.99858E-01 9.99944E-01 9.99980E-01 9.99998E-01 9.99998E-01 1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00	.0000E+00 .0000E+00 .0000E+00 .0000E+00 .0000E+00 .0000E+00 .0000E+00 .0000E+00 .0000E+00	7.66735E+00 8.44469E+00 9.284905E+00 1.02116E+01 1.12007E+01 1.22149E+01 1.31644E+01 1.31644E+01 1.41915E+01 1.38088E+01 1.25690E+01

Argania

57	4.75385E+00	2.89020E+02	2.04895E-01	2.61516E+00	1.00000E+00	1.00000E+00	.00000E+00	1.04835E+01
58	5.18504E+00	2.24582E+02	1.38961E-01	1.32713E+00	1.00000E+00	1.00000E+00	.00000E+00	7.84475E+00
59	5.65501E+00	1.50741E+02	7.94973E-02	5.02584E-01	1.00000E+00	1.00000E+00	•00000E+00	5.19317E+00
60	6.16726E+00	8.67153E+01	3.70889E-02	1.39826E-01	1.00000E+00	1.00000E+00	.00000E+00	3.09693E+00
61	6.72560E+00	4.39682E+01	1.36041E-02	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.82515E+00
	7.33418E+00	4.79473E+01	3.65887E-03	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.24165E+00
62 63	7.99753E+00	5.22841E+01	5.61243E-04	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.04350E+00
		5.70111E+01	3.35954E~05	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00034E+00
64	8.72058E+00			3.02258E-02	1.00000E+00	1.00000E+00	-00000E+00	1.00245E+00
65	9.50870E+00	6.21635E+01	3-43003E-05		1.00000E+00	1.00000E+00	.00000E+00	1.00021E+00
66	1.03678E+01	6.77796E+01	3.25751E-08	3.02258E-02		1.00000E+00	.00000E+00	1.00023E+00
67	1.13041E+01	7.39011E+01	3-26834E-06	3.02258E-02	1.00000E+00	1.00000E+00	-00000E+00	1.00003E+00
68	1.23248E+01	8.05736E+01	3.92039E-08	3.02258E-02	1.00000E+00		*00000E+00	1.00003E+00
69	1.34373E+01	8.78466E+01	4.14188E-07	3.02258E-02	1.00000E+00	1.00000E+00		
70	1.46499E+01	9.57742E+01	5.72454E-08	3.02258E-02	1.00000E+00	1.00000E+00	•00000E+00	1.00000E+00
71	1.59717E+01	1.04415E+02	5.73687E-08	3.02258E-02	1.00000E+00	1.00000E+00	•00000E+00	1.00001E+00
72	1.74124E+01	1.13834E+02	2.42322E-08	3.02258E-02	1.00000E+00	1.00000E+00	*00000E+00	1.00000E+00
73	1.89828E+01	1.24100E+02	4.26732E-09	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
74	2.06945E+01	1.35291E+02	6.87889E-09	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
75	2.25603E+01	1.47488E+02	1.87910E-09	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
76	2.45939E+01	1.60784E+02	8.76048E-10	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
77	2.68107E+01	1.75276E+02	1.00843E-09	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
78	2.92269E+01	1.91072E+02	3.61663E-10	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
79	3.18606E+01	2.08290E+02	7.03837E-11	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
8ó	3.47313E+01	2.27057E+02	1.72169E-10	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
81	3.78604E+01	2.47514E+02	1.16584E-10	3.02258E-02	1.00000E+00	1.0000000+00	-00000E+00	1.00000E+00
	4.12711E+01	2.69811E+02	4.31455E-11	3.02258E-02	1.000005+00	1.00000E+00	.00000E+00	1.00000E+00
82	4.49888E+01	2.94116E+02	1.26455E-12	3.022586-02	1.0000000000	1.00000E+00	.00000E+00	1.00000E+00
83		3.20608E+02	1.12593E-11	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
84 :	4.90411E+01	3.49484E+02	9.64632E-12	3.02258E-02	1.00000E+00	1.00000E+00	-00000E+00	1.00000E+00
85	5.34580E+01				1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
86	5.82725E+01	3.80959E+02	5.02858E-12	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
87	6.35203E+01	4.15266E+02	1.95789E-12	3.02258E-02		1.00000E+00	.00000E+00	1.00000E+00
88	6.92404E+01	4.52662E+02	9.46575E-13	3.02258E-02	1.00000E+00	1.00000E+00	-00000E+00	1.00000E+00
. 89	7.54753E+01	4.934Z3E+0Z	1.11925E-12	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
90	8.22714E+01	5.37852E+02	1.58862E-12	3.02258E-02	1.00000E+00			1.00000E+00
91	8.96791E+01	5.86280E+02	1.89359E-12	3.02258E-02	1.00000E+00	1.00000E+00	•00000E+00	1.00000E+00
92	9.77535E+01	6.39067E+02	1.90321E-12	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
. 93	1.06555E+02	6.96604E+02	1.70387E-12	3.02258E-02	1.00000E+00	1.00000E+00	•00000E+00	1.00000E+00
94	1.16148E+02	7.59320E+02	1.36952E-12	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	
95	1.26604E+02	8.27680E+02	1.05595E-12	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
96	1.38002E+02	9.02193E+02	7.21820E-13	3.02258E-02	1.00000E+00	1.00000E+00	*00000E+00	1.00000E+00
97	1.50425E+02	9.83412E+02	5.37181E-13	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
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99	1.78727E+02	1.16844E+03	2.74865E-13	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
100	1.94816E+02	1.27362E+03	-00000E+00	3.02258E-02	1.00000E+00	1.00000E+00	.00000E+00	1.00000E+00
	207.0202.02							

arm or 3

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                                  AIMFKO =
                                                 .12000
                                                                A2MFK =
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                                  BLTHK =
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27.07989
                                                               DELIN
                                                                              1.18870
     A3MFK =
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     DELTU2 =
                                  DELTU1 =
                                                               DTINC2 =
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                                                                              5.56567
     DTINC1 =
                   5.51352
                                  VEDGE
                                                 .01297
.00426
                                                               NDELTU =
PSI12N =
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                                  PS1120 =
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                                                               PSIZIN =
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                                  PŠIŠŽŇ =
                                                  .00000
                                                               EMFK =
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                                  RTHEAT =8503.50291
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     .97960E+00 5 .47195E+01 .47194E+01 -.60510E+00 -.58989E+00 .84751E+00 .33899E-01 .40399E-03 .16068E-02*** 4490.037
      EDGE QUANTITIES IN VISMFK AT STATION M= 99
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TUZ
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RO2
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                                                                               .00200
                  1.00000
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     RHOE1
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                                  RÕI
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                                                                               .00346
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                                  DELTU1 = YEDGE =
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XC(M).M=1.MMAX (LEVY-LEES STREAMWISE COORDINATE)
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.71534060E+00
.76495067E+00
                                                                                    .60906308E+00
                                                                .60280417E+00
                                                                                                                              .62157658E+00
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                                          - SUMMARY CHART NO. 2
                                                                          ***
              XLE
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56 •775 57 •780 58 •785 59 •790	00 .77500 00 .78500 00 .78500 00 .79500 00 .79500 00 .80500 00 .81000	2.03583 2.06260 2.09311 2.12733	1.38135 1.41236 1.44412 1.47677	14665 13711 12753 11787	1.07082 1.06636 1.06186 1.05729	.04577 .04804 .04973 .05081	.00043 .00045 .00046 .00047	1.00000 1.00000 1.00000 1.00000	4.83073 4.86925 4.88418

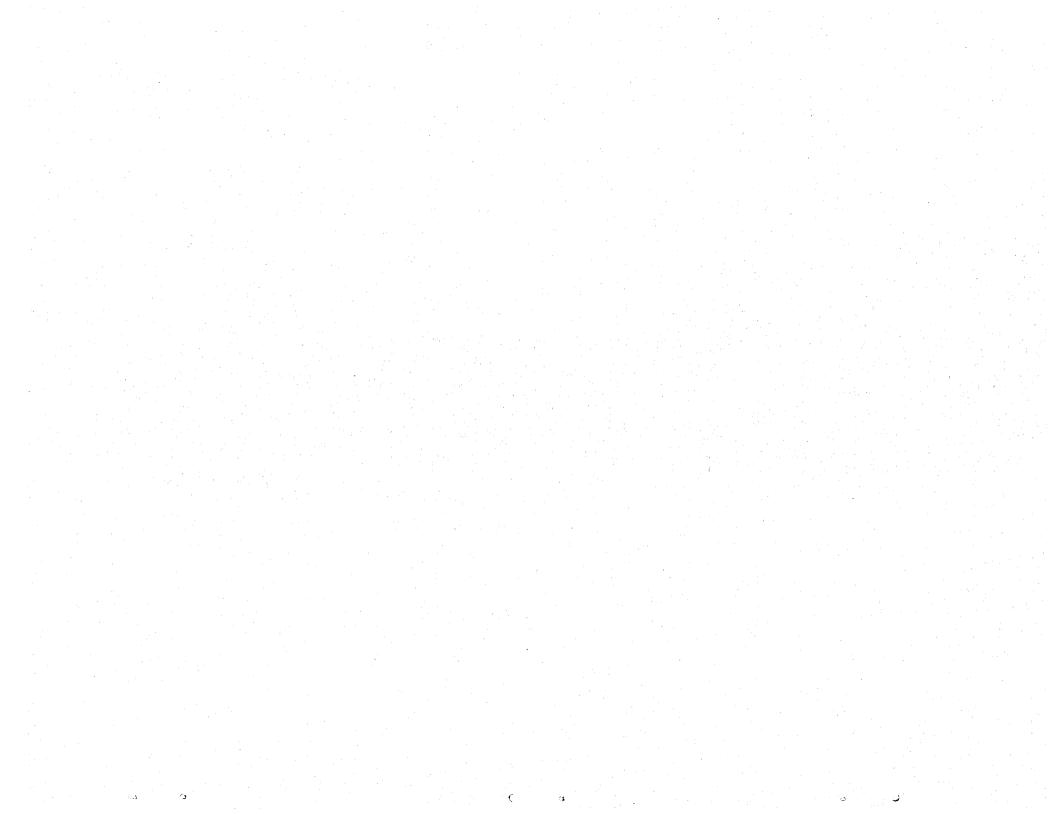
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  .25998520E-02
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                                          .33978774E-02
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                                                                                                    •36593596E-02
                                                                                                                        .37470837E-02
  •38997462E-02
                                         •39924035E-02
OUTPUT QUANTITIES FROM SUBROUTINES INVI & PMFNEW
 VT DISTRIBUTION ON INVISCID MESH AT INTRAC= 40
   .20361118E-01
                                           .67977286E+00
                                                              .82561002E+00
                                                                                  .90943079E+00
                                                                                                     .95978430E+00
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                       .40332743E+00
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   .10165274E+01
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                                          .10359824E+01
                                                                                                                         .11235743E+01
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   .10927839E+01
                       .10979488E+01
                                          •11029631E+01
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   .11339538E+01
                                                                                  .11508377E+01
                                                                                                                         .11568103E+01
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                                                              .11476849E+CI
                                                                                                     .11538151E+01
                       •11391229E+01
                                           .11438725E+C1
                                                                                                                         .11808880E+01
                                                                                                      .11780061E+01
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                                                              .11719349E+C1
                                                                                  .11749757E+01
   •11628612E+C1
                       •11658861E+01
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.1251 .1248 .1232 .1221 .1204 .1047 .1003 .9549	3104E+01 5116E+01 9383E+01 9383E+01 9343E+01 7805E+01 3940E+01 4237E+01 5763E+01 8031E+00 6637E+00	125 124 125 116 107 104 997	520514 513641 482344 212055 555115 78724 7129135 372353	E+01 E+01 E+01 E+01 E+01 E+01 E+00 E+00	.1251 .1247 .1227 .1220 .1123 .1037 .9906 .9436	9143E+0 1867E+0 1315E+0 6072E+0 8249E+0 4099E+0 2463E+0 2463E+0 5690E+0 5690E+0 3023E+0	1	L2509 L2461 L2257 L2204 L1025 L0703 L0319 8426 93804	521E+ 7716E+ 192E+ 1641E+ 1641E+ 1795E+ 1620E+	01 01 01 01 01 01 00 00 00	.125 .124 .122 .109 .106 .102 .978 .932	18283 07085 44160 01018 460861 553861 613998 44638 32862	E+01 E+01 E+01 E+01 E+01 E+01 E+00 E+00	.12 .12 .12 .10 .10 .97 .92	517990 503851 420296 234425 196886 910505 614563 210418 2210418 2214430 732821	E+01 E+01 E+01 E+01 E+01 E+01 E+00 E+00	.12 .12 .12 .10 .10 .10 .96 .92	49988 39174 22704 1898(88429 5691(15389 6465(11233 70384	66E+01 34E+01 47E+01 47E+01 94E+01 98E+01 98E+01 91E+00 91E+00 94E+00	•14 •14 •16 •16 •16 •16 •16 •16 •16 •16 •16 •16	251634 236068 222116556 216556 216556 216556 2165622 207610 207610 207610 207610	0E+01 3E+01 8E+01 5E+01 9E+01 7E+01 8E+00 3E+00	
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			***	SUMM	IARY OF	CONVER	GENCE	HIST	TORY	***				*									
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5	37189E-01	-13632E-02	.99000E+00	-15247E-01	.71776E-03	.69500E+00	-39683E-01	18200E-01	19607E-05
6	-35854E-01	.11859E-02	.70000E+00	.14411E-01	.62002E-03	-69500E+00	.36739E-01	13803E-01	13918E-05
ž	.37338E-01	.12174E-02	.70000E+00	.14568E-01	.57539E-03	.69500E+00	.31468E-01	12110E-01	12308E-05
Ŕ	•37931E-01	.13132E-02	.70000E+00	.14408E-01	.57463E-03	.69000E+00	.19642E-01	11227E-01	11835E-05
ğ	.36763E-01	.13124E-02	.70000E+00	.13543E-01	.55539E-03	.69000E+00	17521E-01	10329E-01	11267E-05
1Ó	•34362E-01	12904E-02	.70000E+00	.12309E-01	•53011E-03	.71500E+00	15959E-01	92950E-02	10419E-05
îĭ	.32601E-01	.12370E-02	.71500E+00	.11606E-01	.49871E-03	.72000E+00	14199E-01	82224E-02	93521E-06
ī 2	.30846E-01	.11607E-02	.71500E+00	•11272E-01	-45899E-03	.72000E+00	•12698E-01	72150E-02	82555E-06
Ī3	.28753E-01	-10808E-02	.71500E+00	.10797E-01	.42061E-03	.72000E+00	.12454E-01	63217E-02	73701E-06
14	.27811E-01	-10097E-02	.72000E+00	.10195E-01	•38668E-03	.72000E+00	•11888E-01	55837E-02	65829E-06
- 15	•26834E-01	.94115E-03	•72000E+00	•95929E-02	.35684E-03	.72000E+00	.11046E-01	50729E-02	58908E-06
16	.25518E-01	.88249E-03	•72000E+00	.89118E-02	•32869E-03	.72000E+00	•11266E-01	46236E-02	52969E-06
· 17	•24144E-01	.81540E-03	.72000E+00	.82517E-02	•30262E-03	.72000E+00	.10800E-01	42768E-02	47811E-06
18	.22876E-01	.75540E-03	.72000E+00	•76635E-02	.27832E-03	.72000E+00	.96507E-02	39384E-02	43234E-06
· 19	•21520E-01	.70657E-03	•72000E+00	.70771E-02	.25811E-03	•72000E+00	.86351E-02	36242E-02	39763E-06
20	.20079E-01	.66051E-03	•72000E+00	•65114E-02	.23938E-03	.72500E+00	.80968E-02	33412E-02	36725E-06
Ž1	•18670E-01	.61709E-03	•72000E+00	.61158E-02	.22284E-03	.72500E+00	•715 <u>3</u> 2E-02	30799E-02	33911E-06
22	•17102E-01	.56734E-03	•72000E+00	.56481E-02	.20331E-03	.72500E+00	•74374E-02	28243E-02	31257E-06
23	•15729E-01	•53562E-03	•72000E+00	•51653E-02	•18857E-03	•72500E+00	•77529E-02	25995E-02	28732E-06
24	•14475E-01	.48719E-03	•72000E+00	.48521E-02	•17264E-03	•72500E+00	•66125E-02	23813E-02	26313E-06
25	•13247E-01	•44865E-03	•72000E+00	•45232E-02	•15824E-03	.72500E+00	•56307E-02	21597E-02	24061E-06
26	•12280E-01	.41280E-03	• 72500E+00	42223E-02	.14514E-03	•72500E+00	•51374E-02	19829E-02	21966E-06
27	•11568E-01	•38134E-03	•72500E+00	• 3935 EE-02	•13338E-03	•72500E+00	.46418E-02	18097E-02	20056E-06
28	-10842E-01	•35872E-03	•72500E+00	•36530E-02	.12470E-03	•72500E+00	-42247E-02	1655 QE-02	18333E-06
29	•98367E-02	•33623E-03	•72500E+00	•32849E-02	•11549E-03	•72500E+00	•51801E-02	15167E-02	16781E-06
30	•91480E-02	-30044E-03	•72500E+00	•30302E-02	•10433E-03	•72500E+00	•42259E-02	13856E-02	15358E-06
31	•85574E-02	.27128E-03	•72500E+00	.28134E-02	-94150E-04	•72500E+00	•37165E-02	12502E-02	13986E-06
32	-81339E-02	.24926E-03	•72500E+00	• 26553E-02	.86780E-04	•72500E+00	•26145E-02	13246E-02 10457E-02	12699E-06 11574E-06
33	•75886E-02	•23308E-03	•72500E+00	•24611E-02	-80134E-04	•72500E+00	•30114E-02		11574E-06
34	•70868E-02	•21603E-03	•72500E+00	•22844E-02	•74176E-04	•72500E+00	.26354E-02 .24816E-02	96796E-03	97452E-07
35	•65908E-02	•20105E-03	•72500E+00	•21126E-02	.68885E-04 .63367E-04	.72500E+00	.24263E-02	83048E-03	89640E-07
36	•61362E=02	•18479E-03	•72500E+00	•19566E-02	.58632E-04	.72500E+00	.23070E-02	77849E-03	82478E-07
37	•57149E-02	•17140E-03 •15876E-03	•72500E+00 •72500E+00	•18135E-02 •16805E-02	.54246E-04	•72500E+00	.20079E-02	75394E-03	75880E-07
38 39	•53196E-02	•19876E-03	• 72500E+00	•15228E-02	.50772E-04	•72500E+00	.19500E-02	64088E-03	69885E-07
40	•48401E-02 •44969E-02		.72500E+00	.14095E-02	.45920E-04	.72500E+00	.17686E-02	65451E-03	64283E-07
+ U	• 44404E=02	•13448E-03	• 12300ET00	• 14073E-02	• 473505-04	• 1 Z J S O E + O O	• T1000E-02		10.2036-01

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ALESEP: A Computer Proc	ram for the Analys	sis of Ai	rfoil -	April 19							
Separation Bubbles	grant for the Palary.)1D OI 11	6	. Performing (Organization Code						
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15. Supplementary Notes											
	.										
Langley Technical Monito	or: Joel L. Everh	art									
16. Abstract											
A program called ALESEP	is presented for	the analy	sis of th	e invisc	id-viscous inter-						
action which occurs due	- .										
bubble on an airfoil.											
layer equations expresse					. = 1						
			-		1						
representation of the ir				-							
local perturbation to a					-						
hence, part of the requi	_ ·				-						
thickness and tangential											
may be used in the rever	rsed flow regions (of the se	eparation	bubble to	o accurately						
account for the flow dir	rection in the dis	cretizati	ion of the	streamw:	ise convection						
of momentum. The ALESEI	code contains bo	th a forc	ced transi	tion mode	el based on a						
streamwise intermittency	function and a n	atural tr	cansition	model bas	sed on a solution						
of the integral form of	the turbulent kind	etic ener	av equati	on. Inst	tructions for the						
input, output, and progr											
					,						
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17. Key Words (Suggested by Author(s))	T	10 Distribus	on Statement								
Interaction, Separation	Rubble Viccous			IIm I dan da	ä						
	· ·	Olicida	ssified -	ourmirre	٦						
Transitional, Airfoil Se	shara cron										
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Unclassified	Unclassified	1									



